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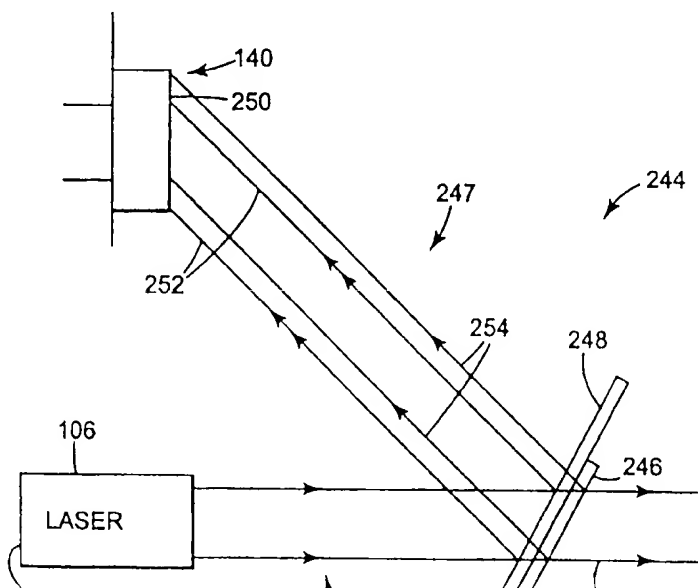
## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

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(54) Title: OPTICAL SCANNER FEEDBACK SYSTEM

## (57) Abstract

An optical scanner feedback system (244). The feedback system (244) provides a feedback signal representative of a laser beam (88) focused along an optical path onto a scanning surface (66). The feedback system (244) includes a cylinder lens (L1) having a longitudinal axis (202a) and a transverse axis (203a), located along the optical path having an optical surface for shaping and focusing the laser beam in a first direction. A photodetector (140) is provided having an active region (250) sensitive to light. The laser beam (88) includes a scanning portion which passes through the lens (L1) and a reflected portion (247) which reflects off the lens (L1). The reflected portion (247) is reflected such that it is incident on the photodetector (140) active region (250) for providing an output signal representative of the laser beam (88).



OPTICAL SCANNER FEEDBACK SYSTEMBackground of the Invention

5 The present invention relates generally to optical scanner assemblies and laser imaging systems incorporating such scanners. In particular, the present invention relates to a lens feedback system suitable for use in an internal drum type optical scanner assembly.

10 Laser imaging systems are commonly used to produce photographic images from digital image data generated by magnetic resonance (MR), computed tomography (CT) or other types of scanners. Systems of this type typically include a continuous tone laser imager for exposing the image on photosensitive film, a film  
15 processor for developing the film, and an image management subsystem for coordinating the operation of the laser imager and the film processor.

The digital image data is a sequence of digital  
20 image values representative of the scanned image. Image processing electronics within the image management subsystem processes the image data values to generate a sequence of digital laser drive values (i.e., exposure values), which are input to a laser  
25 scanner. The laser scanner is responsive to the digital laser drive values for scanning across the photosensitive film in a raster pattern for exposing the image on the film. The continuous-tone images used in the medical imaging field have very stringent image-  
30 quality requirements. A laser imager printing onto transparency film exposes an image in a raster format, the line spacing of which must be controlled to better than one micrometer. In addition, the image must be uniformly exposed such that the observer cannot notice  
35 any artifacts. In the case of medical imaging, the

Optical scanning assemblies are used to provide uniform exposure of the image on photosensitive film. The optical scanning assemblies combine a laser system with unique optical configurations (i.e., lenses and mirrors), for uniform exposure of the image onto the film. Past optical scanning assemblies used for achieving the level of performance required by the medical imaging industry utilize costly components incorporated into complex optical scanning systems. Such systems often combine complex, multi-sided mirrors and lens configurations for directing the laser beam onto a moving or stationary photosensitive film.

Known laser imagers used for medical imaging include a polygonal scanner or a galvanometer scanner. For example, a commonly used polygonal scanner configuration has a polygonal mirror repetitively exposing successive raster lines onto a sheet of moving photosensitive film. The optics must focus the laser beam over a flat image line and compensate for facet-to-facet angular errors in the polygon. These functions have usually been accomplished with combinations of costly precision ground anti-reflection coated glass lenses. The film is moved at a constant speed on rollers where the film is placed at the focus of the scanning laser beam. The film must be moved with a surface velocity constant to better than about 0.5%. Momentary disturbances or perturbations in the motion of the film, such as those caused by striking a film guide, position sensor or nip roller, can cause serious "glitches" in the exposed image, resulting in poor image quality. Avoidance of such perturbations requires that the film path during imaging be free of such obstructions. Such a film path often occupies a considerable amount of space in the laser imaging device.

scanner assembly having a dual-galvanometer configuration. The dual-galvanometer configuration includes one galvanometer mirror which repetitively sweeps the laser beam to form the raster lines, while a  
5 second, slower-moving galvanometer mirror deflects the raster lines down the page of the photographic film. The film, held motionless during exposure, is usually held in a curved platen to avoid the necessity of flattening the image field in both directions. While  
10 problems due to film motion are eliminated, since the film can be curved in only one direction at once, such a configuration requires the use of field-flattening optics for its operation. The use of galvanometers, on the other hand, offers relief from the problem of  
15 facet-to-facet errors found in polygon-based scanner systems. Galvanometers, like accurate polygon spinners, are precision instruments, and therefore, are very expensive to manufacture.

In light of the known drawbacks of present laser  
20 imaging devices, it is desirable to have an optical scanner which does not rely on expensive mirror and optical configurations to compensate for errors inherent in the scanner design. It is desirable to have an optical scanner for use in a laser imager which  
25 does not require an extraordinary amount of space nor which requires space considerations due to the introduction of glitches from the film path. Further, it is desirable to have an optical scanner for use with a laser imager which meets the image-quality  
30 requirements of the medical imaging industry.

#### Summary of the Invention

The present invention is directed to a lens  
feedback system and an optical scanner assembly having  
35 a lens feedback system for use in a laser imager. The

medical imaging industry. Further, the novel configuration of the optical scanner lens feedback system in accordance with the present invention allows a common lens to be used for focusing and shaping the laser beam and as a beam splitter for providing a laser beam feedback signal representative of the laser beam.

In one embodiment, the present invention includes a feedback system for providing a feedback signal representative of a laser beam focused along an optical path onto a scanning surface. The feedback system includes a cylinder lens having a longitudinal axis and a transverse axis, located along the optical path, having an optical surface for shaping and focusing the laser beam in a first direction. A photodetector is provided having an active region sensitive to light. The laser beam includes a scanning portion which passes through the cylinder lens and a reflected portion which reflects off of the lens. The reflected portion is reflected such that it is incident on the photodetector active region. The photodetector active region is responsive to the reflected portion for providing an output signal representative of the laser beam.

The cylinder lens is angled such that the reflected portion is incident on the active region. The cylinder lens transverse axis is perpendicular to the optical path. The cylinder lens is rotated about the transverse axis, such that the cylinder lens longitudinal axis is not perpendicular to the optical path.

In one application, the lens is a plano-convex cylinder lens. The cylinder lens may include a flat, partially reflective surface and a curved, partially reflective surface. The curved surface is located between the flat surface and the scanning surface. The reflected portion includes a first reflected beam

partially reflective surface. The system may further include a second cylinder lens located along the optical path oriented generally perpendicular to the first cylinder lens for shaping and focusing the laser beam in a second direction.

In another exemplary embodiment, the present invention includes a laser feedback control system for use in a laser imaging system. The laser feedback control system includes a laser assembly for producing a laser beam representative of the image to be exposed on the photosensitive film. A cylinder lens having a longitudinal axis and a transverse axis is positioned in optical alignment along an optical path as defined by the laser beam, for focusing and shaping the laser beam. A photodetector is provided having an active region sensitive to a laser light. The laser beam includes a reflected portion which is reflected off of the cylinder lens and which does not pass through the cylinder lens. The reflected portion is directed to be incident on the photodetector active region. The photodetector active region is responsive to the reflected portion for providing an output signal representative of the laser beam.

The system further includes a laser driver, wherein the laser driver is responsive to the output signal for providing a modulated laser beam output signal. The system may further include a controller, wherein the controller provides an image signal to the laser driver, wherein the laser driver is responsive to the output signal and the image signal for modulating of the laser beam. The cylinder lens is tilted relative to the optical path for directing the reflected portion to be incident on the photodetector active region. The angle between the cylinder lens and the optical path defines a tilting angle, wherein the

In one preferred application, the cylinder lens is a plan-convex cylinder lens. The plano-convex cylinder lens includes a flat surface and a curved surface, and the curved surface is between the flat surface and the scanning surface, and wherein the reflected portion includes a first reflected laser beam, which reflects off of the flat surface, and a second reflected laser beam which reflects off of the curved surface. The photodetector active region has a size sufficient to receive the first reflected laser beam and the second reflected laser beam. The cylinder lens transverse axis is perpendicular to the optical path, and the cylinder lens longitudinal axis is not perpendicular to the optical path. A second cylinder lens may be further provided having a longitudinal axis and a transverse axis, wherein the second cylinder lens transverse axis is oriented substantially perpendicular to the first cylinder lens transverse axis, positioned along the optical path for shaping and focusing the laser beam in a direction different from the first cylinder lens. In one embodiment, the reflected portion represents less than 10 percent of the laser beam.

In yet another exemplary embodiment, the present invention includes a laser scanning assembly for exposing an image on a scanned surface. The laser scanning assembly includes a laser assembly for producing a laser beam representative of the image to be exposed on the scan surface. The laser beam defines an optical path between the laser assembly and the scan surface. A first lens system is positioned in optical alignment along the optical path including a cylinder lens positioned in optical alignment along the optical path for focusing and shaping the laser beam in a first direction. A second lens system is provided for

is located along the optical path. A photodetection mechanism is provided, wherein the laser beam includes a reflected portion which is reflected off of the cylinder lens, wherein the reflected portion is  
5 directed to be incident on the photodetection mechanism. The photodetection mechanism is responsive to the reflected portion for providing an output signal representative of the laser beam. A controller may be provided which is responsive to the output signal for  
10 providing a laser beam modulation signal to the laser assembly.

#### Brief Description of the Drawings

Fig. 1 is an elevational diagram of a laser  
15 imaging apparatus in accordance with the present invention;

Fig. 2 is a perspective view of an exemplary film exposure assembly having an optical scanner assembly for use in a laser imaging apparatus, in accordance  
20 with the present invention;

Fig. 3 is an end view of the film exposure assembly shown in Fig. 2;

Fig. 4 is a block diagram illustrating an exemplary optical scanner assembly laser beam shaping  
25 and directing system in accordance with the present invention;

Fig. 5 is a perspective view of one exemplary embodiment of an optical scanner assembly laser beam shaping and directing system in accordance with the  
30 present invention;

Fig. 6 is an optical diagram in the cross-scan direction illustrating an exemplary embodiment of the optical scanner laser beam shaping and directing system shown in Fig. 5;

35 Fig. 7 is an optical diagram in the cross-scan



directing system shown in Fig. 5;

Fig. 8 is an optical diagram in the in-scan direction illustrating an exemplary embodiment of the optical scanner assembly laser beam shaping and  
5 directing system shown in Fig. 5;

Fig. 9 illustrates an exemplary embodiment of an optical configuration suitable for use in an optical scanner assembly in accordance with the present invention;

10 Fig. 9a is a perspective diagram illustrating the orientation of lens L1 and lens L2;

Fig. 10 is a graph illustrating focal length versus tilt angle for one exemplary embodiment of a lens in Fig. 9;

15 Fig. 11 is a cross-sectional view of one exemplary embodiment of a lens shown in Fig. 9;

Fig. 12 is a longitudinal cross-sectional view of an exemplary embodiment of a lens shown in Fig. 9;

20 Fig. 13 is a perspective view illustrating a step in a manufacturing process of forming a lens shown in Fig. 9;

Fig. 14 is a perspective view illustrating another step in a manufacturing process of forming a lens shown in Fig. 9;

25 Fig. 15 is a perspective view illustrating another step in a manufacturing process of forming a lens shown in Fig. 9;

Fig. 16 is a block diagram illustrating an exemplary embodiment of a laser beam feedback control system for use in an optical scanner system, in  
30 accordance with the present invention;

Fig. 17 is a top view of an exemplary embodiment of the use of a lens as a beamsplitter in a laser feedback control system, in accordance with the present  
35 invention is shown;

laser feedback control system, in accordance with the present invention;

Fig. 19 a top perspective view of an exemplary embodiment of a flexible cylinder lens in accordance  
5 with the present invention;

Fig. 20 illustrates an edge view of the flexible cylinder lens shown in Fig. 19 in a curved position;

Fig. 21 illustrates another exemplary embodiment of an edge view of the flexible cylinder lens shown in  
10 Fig. 19 in a flexed or curved position;

Fig. 22 is a cross-sectional view of one exemplary embodiment of the flexible cylinder lens illustrated in Fig. 19;

Fig. 23 illustrates a longitudinal cross-sectional  
15 view of an exemplary embodiment of the flexible cylinder lens shown in Fig. 19;

Fig. 24 is a perspective view illustrating an exemplary embodiment of a step in a manufacturing process of forming the lens shown in Fig. 19;

20 Fig. 25 is a perspective view illustrating an exemplary embodiment of another step in a manufacturing process of forming the lens shown in Fig. 19;

Fig. 26 is a perspective view illustrating an exemplary embodiment of another step in a manufacturing  
25 process of forming the lens shown in Fig. 19;

Fig. 27 is a perspective view illustrating an exemplary embodiment of another step in a manufacturing process of forming the lens shown in Fig. 19;

30 Fig. 28 is a perspective view illustrating an exemplary embodiment of another step in a manufacturing process of forming the lens shown in Fig. 19;

Fig. 29 is a perspective view illustrating an exemplary embodiment of another step in a manufacturing process of forming the lens shown in Fig. 19;

35 Fig. 30 is a perspective view illustrating an

Fig. 31 is a perspective view illustrating an exemplary embodiment of another step in a manufacturing process of forming the lens shown in Fig. 19;

Fig. 32 illustrates a perspective view of an exemplary embodiment of an attenuator for use with an optical scanner assembly, in accordance with the present invention;

Fig. 33 is a top view of the attenuator shown in Fig. 32;

Fig. 34 illustrates a longitudinal cross-sectional view of one embodiment of the attenuator in accordance with the present invention, taken along line 34-34 of Fig. 33;

Fig. 35 is a graph of optical density versus distance for one exemplary embodiment of the attenuator shown in Fig. 33;

Fig. 36 is an optical diagram illustrating an exemplary embodiment of the effect of a laser beam passing through the attenuator in accordance with the present invention;

Fig. 37 is a graph illustrating an exemplary embodiment of the intensity of the laser beam relative to a center axis before it passes through the attenuator shown in Fig. 36;

Fig. 38 is a graph illustrating an exemplary embodiment of the intensity of the laser beam relative to a center axis after it passes through the attenuator shown in Fig. 36;

Fig. 39 is a block diagram illustrating one exemplary embodiment of a motor control system for calibration of an attenuator in accordance with the present invention;

Fig. 40 is a first perspective view illustrating an exemplary embodiment of an optical scanner assembly for use in a laser imager in accordance with the

40; and

Fig. 42 is a block diagram illustrating one exemplary embodiment of operation of an optical scanner assembly in accordance with the present invention.

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#### Detailed Description of the Preferred Embodiments

Figure 1 is an elevational diagram illustrating an exemplary embodiment of a laser imaging system 30 suitable for use in the medical imaging industry including an optical scanner assembly, in accordance with the present invention. The imaging system 30 includes a film supply mechanism 32, a film exposure assembly 34, a film processing station 36, a film receiving area 38, and a film transport system 40. The film supply mechanism 32, film exposure assembly 34, film processing station 36, and film transport system 40 are all located within an imaging system housing 42.

Photosensitive film is stored within the film supply mechanism 32. The film transport system 40 allows the photosensitive film to be moved between the film exposure assembly 34, film processing station 36, and the film receiving area 38. The film transport system 40 may include a roller system (not shown) to aid in transporting the film along a film transport path, indicated by dashed line 44. The direction of film transport along film transport path 44 is indicated by arrows 46. In particular, the film supply mechanism 32 includes a mechanism (not shown) for feeding a piece of film along film transport path 44 into the film exposure assembly 34 for exposing the desired image on the photosensitive film using the optical scanner assembly in accordance with the present invention. After exposure of the desired image on the photosensitive film, the photosensitive film is moved along the film transport path 44 to the film processing

the image on the photosensitive film. After film development, the photosensitive film is transported to the film receiving area 38.

In Figure 2, a top perspective view of one  
5 exemplary embodiment of the film exposure assembly 34 including an optical scanner assembly in accordance with the present invention is shown. The film exposure assembly 34 has an internal-drum type configuration. In the exemplary embodiment shown, the film exposure  
10 assembly 34 includes an optical scanner assembly 50 (better seen in Fig. 3) mechanically coupled to an optics translation system 52, mounted within drum 54 for exposure of the film. The center of curvature of the drum 54, which is located along the drum  
15 longitudinal axis, is indicated by dashed line 56. During a scanning process, the optics translation system 52 operates to move the optical scanner assembly 50 along the longitudinal axis 56, indicated by directional arrow 58, and after scanning, returns the  
20 optical scanner assembly 50 to a start position, along the longitudinal axis 56, indicated by directional arrow 60.

Referring also to Figure 3, an end elevational view of the film exposure assembly 34 is shown. Drum  
25 54 includes a film platen 62 having an internal drum surface 64. During exposure of a photosensitive film 66, the photosensitive film 66 is held against the internal drum surface 64, which has a cylindrical or partial cylindrical shape.

30 In general, the photosensitive film 66 is held against the film platen internal drum surface. The optical scanner assembly 50 scanning laser beam (indicated at 68) emanates radially from the center of curvature of the drum 54, which is located along the  
35 drum longitudinal axis 56. The optical scanner

lines by rotating about the longitudinal axis 56 of the cylinder drum. As the optical scanner assembly 56 scans the image in raster lines on photosensitive film 66 located on the internal surface of the drum 64, the optics translation system 52 moves the optical scanner assembly 50 along the longitudinal axis 56 to expose the full image on the photosensitive film. The optical scanner assembly in accordance with the present invention is described in detail later in this specification.

In one exemplary embodiment, the film exposure area on the internal drum surface is 17 (43.2 cm) inches by 14 inches (35.6 cm), suitable for exposure of a 17 inch (43.2 cm) by 14 inch (35.6 cm) piece of photosensitive film. In the exemplary embodiment disclosed herein, the film is exposed in a vertical direction. In particular, since the 14 inch (35.6 cm) edge of the film is fed into the exposure module and subsequently scanned in the 17 inch (43.2 cm) direction, the scanned raster lines appear in the vertical direction. The laser beam is scanned 180° across the internal drum surface, for exposure of 17 inches (43.2 cm) across the photosensitive film. The optics translation system moves the optical scanner assembly along the longitudinal axis located at the center of curvature of the internal drum surface for a distance of 14 inches (35.6 cm), for full exposure of the desired image/images on photosensitive film.

The photosensitive film can be a photosensitive film which is sensitive to laser beam light. In one exemplary embodiment, the film is a light sensitive photothermographic film having a polymer or paper base coated with an emulsion of dry silver or other heat sensitive material. One known film suitable for use in medical imaging is

commercially available under the tradename Dryview Imaging Film (DVB or DVC), manufactured by Imation Corp. of Oakdale, Minnesota.

5 The optical scanner assembly, components of the optical scanner assembly, and operation of the optical scanner assembly are described in detail in the following paragraphs.

#### **Optical Scanner Assembly**

##### **1. Laser Beam Shaping and Directing System.**

10 The optical scanner assembly in accordance with the present invention includes a laser beam shaping and directing system. In Figure 4, a block diagram of one exemplary embodiment of a laser beam shaping and directing system in accordance with the present  
15 invention is generally shown at 70. As shown in Figure 4, the laser beam shaping and directing system includes a controller 72, a laser driver 74, a laser assembly 76, first optical mechanism 78, second optical mechanism 80, a scanning and directing system 82  
20 positioned in optical alignment with photosensitive film 66. Controller 72 provides an image signal 84 to laser driver 74 representative of the image to be exposed on the photosensitive film 66. Controller 72 also provides control signals to and receives control  
25 signals from scanning and directing system 82, indicated at 85. Laser driver 74 is responsive to image signal 84 for providing an output driver signal 86 to laser assembly 76. In response to output driver signal 86, laser assembly 76 emits (produces) a laser  
30 beam which is representative of the image to be exposed on the photosensitive film 66. The first optical mechanism 78, second optical mechanism 80 and scanning and directing system 82 function together to shape, focus, and direct the laser beam 88 for exposing the  
35 desired image or images on the photosensitive film 66

directions, which are generally perpendicular to each other. The first optical mechanism 78 includes a lens system which functions to shape the laser beam 88 profile in a first direction (but not a second  
5 direction) for focusing the laser beam 88 in a first direction on the film 66. The second optical mechanism 80 includes a lens system which functions to shape the laser beam 88 in the second direction (but not the first direction) for focusing the laser beam 88 in the  
10 second direction onto the photosensitive film 66. Scanning and directing system 82 includes a scanner and mirror system for directing the laser beam 88 to the desired location on film 66 and scanning the laser beam 88 across the film surface in a raster pattern for  
15 exposing the desired image on film 66.

In Figure 5, a perspective view of one exemplary embodiment of an optical scanner assembly laser beam shaping and directing system in accordance with the present invention is generally shown. As shown in  
20 Figure 5, the laser beam shaping and directing system 70 includes a laser diode 132, a laser collimator 134, a lens L1, a lens L2, a folding mirror M1, a scanner assembly 136, including a scanner motor 138 and a scanner mirror M2, a flexible lens L3, a feedback  
25 sensor 140, an absorbing surface 142, and an absorbing surface 144. As shown in Figure 5, laser diode 132 and laser collimator 134 comprise the laser assembly 76. First optical mechanism 78 includes lens L1 and lens L3. Second optical mechanism 80 includes lens L2. The  
30 scanning and directing system 82 includes folding mirror M1 and scanner assembly 136, including scanner motor 138 and scanner mirror M2.

Laser diode 132, laser collimator 134, lens L1, lens L2, folding mirror M1, scanner mirror M2, and  
35 flexible lens L3 are in optical alignment (along a path



photosensitive film. In the particular embodiment shown, lens L1 is optically positioned between lens L2 and laser collimator 134. Lens L2 is optically positioned between lens L1 and folding mirror M1.

5 Folding mirror M1 is optically positioned between lens L2 and scanner mirror M2. Scanner mirror M2 is optically positioned between folding mirror M1 and lens L3. Lens L3 is optically positioned between scanner mirror M2 and the film 66. It is recognized that the  
10 above laser beam shaping and directing system 70 elements may be alternately configured within the scope of the present invention, such as lens L2 being in optical alignment between collimator 134 and lens L1, and lens L1 being in optical alignment between lens L2  
15 and folding mirror M1.

In summary, the laser diode 132 is electrically coupled to laser driver 104 (shown in Figure 4). The laser diode 132 emits laser beam 88 through laser  
collimator 134 such that the collimated laser beam 88  
20 is a uniformly shaped light source (modulated in an image-wise pattern), representative of the image to be exposed on the film. In one preferred embodiment, the collimated laser beam 88 is generally elliptical shaped.

25 The laser beam 88 is transmitted through lens L1, transmitted through lens L2 and is reflected by the folding mirror M1 such that it is incident on the scanner mirror M2. In one preferred embodiment, the scanner mirror M2 is a two-sided mirror which is  
30 mounted on the shaft through an adapter 137 of scanner motor 138. In one embodiment, the scanner motor 138 is a DC brushless motor.

Upon operation of scanner motor 138, the scanner mirror M2 is rotated and the laser beam 88 is reflected  
35 outward radially in an approximate conical shape and

mirror M2 are used for directing the laser beam 88 through flexible lens L3 to expose the film 66. In one embodiment, the laser beam 88 and the motor axis form an angle that is nominally  $84^\circ$ .

5 In one exemplary embodiment, lens L1, lens L2, and flexible lens L3 are cylinder lenses, and in particular, are cylinder lenses having a plano-convex optical configuration. A plano-convex cylinder lens is a lens having a straight side (i.e., planar) and a  
10 convex or curved opposite side. Lens L1 has its convex side facing lens L2. Lens L2 has its convex side facing folding mirror M1, and flexible lens L3 has its convex side facing the film 66. Lens L1 and lens L2 are positioned such that the focusing directions are  
15 perpendicular to each other, and as such, lens L1 shapes laser beam 88 in the cross-scan direction, and lens L2 shapes laser beam 88 in the in-scan direction.

Each of these lenses and the effect of their orientation will be described in detail later in the  
20 specification.

With the present invention, all of the optical elements, including lens L1, lens L2 and flexible lens L3, are tilted from a perpendicular position relative to the optical axis. As such, all of the reflected  
25 beams (reflected portions of the laser beam) can be controlled such that they are dumped onto absorbing surfaces to eliminate light scattering from reflected beams or otherwise used. By controlling the reflected beams, lens L1, lens L2, and flexible lens L3 do not  
30 require costly anti-reflective coatings.

In particular, lens L1 and lens L2 are tilted relative to an optical path defined by the laser beam 88. In particular, lens L1 and lens L2 each include a longitudinal axis and a transverse axes extending  
35 perpendicular to the longitudinal axis. The transverse axes of lens L1 and lens L2 are perpendicular to each other.

optical path. The lens L1 and lens L2 longitudinal axes are not perpendicular to the optical path, being angled or "tilted", and are rotated about their respective transverse axis. As will be described later  
5 in the specification, the tilt in lens L2 may be used to aid in focusing laser beam 88 at a desired location (for the scanned surface). Further, the reflected beam from tilted lens L1 provides a feedback signal 147 to feedback sensor 140. Operation of the lens feedback  
10 system will also be described later in the specification. Lens L2 is also tilted to allow a portion of the laser beam 88 which reflects off the surface of the lens L2, indicated as reflected beam 146, to be dumped onto absorbing surface 142, such that  
15 it does not generate undesirable stray light or spurious film exposures.

Flexible lens L3 is tilted from a perpendicular position relative to the optical axis as defined by the laser beam. As such, a portion of laser beam 88  
20 reflects off of flexible lens L3, indicated at 148, and is dumped onto another absorbing surface 144 instead of reflecting directly back into the optics module. Similarly, the optical axis of the laser beam 88 passing through flexible lens L3 is not perpendicular  
25 to the position of the film, and as such, the reflected beam 147 from the film is also dumped to an absorbing surface 149 to avoid light scattering. In one embodiment, the incident angle of the laser beam 88 relative to an axis perpendicular to the flexible lens  
30 L3 and the film is nominally 6°.

In Figure 6, an optical diagram illustrating beam shaping in the cross-scan direction is shown. In the exemplary embodiment shown, lens L1 and flexible lens L3 cooperate to focus the laser beam 88 on the film 66

representative of the image to be formed on  
photosensitive film 66, indicated at 152. As laser  
beam 88 passes through lens L1 (153), lens L1 acts to  
focus the laser beam 88 at the position of the spinning  
5 mirror M2 (156). As such, mirror M2 is said to be  
located a distance  $f_1$  from lens L1, where  $f_1$  is  
representative of the focal length of lens L1. Between  
lens L1 and mirror M2, laser beam 88 passes through  
lens L2, indicated at 154. Due to the orientation of  
10 lens L2 (L2 is a cylinder lens positioned such that its  
focusing direction is generally perpendicular to the  
focusing direction of lens L1), lens L2 does not effect  
the shape of laser beam 88 in the cross-scan direction.

Additionally, folding mirror M1 (155) acts to direct  
15 laser beam 88 at scanner mirror M2.

Scanner mirror M2 rotates to scan laser beam 88 in  
a raster pattern across the surface of film 66.

Located half-way (proximate the midpoint) between  
scanner mirror M2 and the film 66 is flexible lens L3.

20 In particular, flexible lens L3 is located at a  
distance which is twice the focal length ( $2f_3$ ) of  
flexible lens L3, and the film 66 is located a distance  
from flexible lens L3 which is also twice the focal  
length ( $2f_3$ ) of flexible lens L3. As such, mirror M2  
25 and the photosensitive film 66 are located at the  
conjugate points of flexible lens L3.

In Figure 7, an enlarged optical diagram showing  
one exemplary embodiment of the relationship between  
scanner mirror M2, flexible lens L3 and the film 66 in  
30 the cross-scan direction is shown. The novel optical  
configuration in accordance with the present invention,  
including the positioning of flexible lens L3 between  
scanner mirror M2 and the film (or scanned) plane 66  
may also operate as a mechanism or means for wobble

that it may cause artifacts in the image exposed on the film 66. For example, assuming an optical pointing angle error of 10 arcsec and a distance of 137 mm between the scanner mirror and the film, the wobble at the film is 6.6 micrometers.

As shown in Figure 7, the beam wobble is depicted by directional arrow 162. A number of items may contribute to beam wobble. For example, in addition to beam wobble due to mirror pointing errors, the scanner motor 138 shaft may wobble (possibly due to bearing tolerance), which contributes to the overall beam wobble at the film plane 66.

The novel optical configuration including flexible lens L3 is used as a mechanism or means for wobble correction. The laser beam 88 is focused to a line on the scanner mirror M2, narrower in the cross-scan direction, which is re-imaged to the film 66 through flexible lens L3 (indicated at 164). As previously described herein, the laser beam 88 may wobble, indicated by directional arrow 162. As such, the optical path of laser beam 88 between mirror M2 and the film 66 is adjusted by flexible lens L3, indicated by dashed lines 166. Flexible lens L3 operates to redirect the displaced laser beam 166 to the desired location on film 172, indicated at 164. Due to the plano-convex flexible lens L3, even if the laser beam 88 is shifted due to wobble effects, flexible lens L3 redirects the laser beam 88 to the desired location 164 on film 66. As such, flexible lens L3 provides for correction for beam wobble.

In Figure 8, an optical diagram illustrating operation of the novel lens configuration in the in-scan direction, in accordance with the present invention, is generally shown at 170. Collimated laser beam 88 (at 172) is emitted from laser assembly 76 and

affect the shape of laser beam 88. Lens L2 operates to focus the laser beam 88 in the in-scan direction onto the film 66. As such, the distance between lens L2 and the film 66 is equal to the focal length  $f_2$  of the lens L2.

Between lens L2 and the film 66, the laser beam 88 is redirected by mirror M1 (at 178) to the rotating scanner mirror M2 (at 180). The rotating scanner mirror M2 directs the laser beam 88 along a scan line 184 across the film plane 66 as it rotates. In Figure 8, the laser beam 88 is shown in a first position 186, and a second rotated position 188, relative to the first position 186. As the rotating scanner mirror M2 scans the laser beam 88 in the in-scan direction, the laser beam 88 passes through flexible lens L3 (at 182).

Flexible lens L3 does not affect the shape of laser beam 88 in the in-scan direction.

In one exemplary embodiment, the laser beam 88 exiting the laser assembly 76 collimator 134 has an elliptical shape, with  $1/e^2$  diameters of approximately 1.1 mm and 4.0 mm in the cross-scan and in-scan directions, respectively. In the cross-scan direction, the laser beam 88 is focused by L1,  $f_1=95.6$  mm onto the scanner mirror M2 surface. The image on the scanner mirror M2 surface is imaged through the flexible lens L3, having a focal length  $f_3$  equal to 34.1 mm, onto the film 66. In the in-scan direction, cylindrical lens L2 having a focal length  $f_2$  equals 192 mm, focuses the collimated laser beam 88 to the film plane 66 directly.

In one preferred embodiment, the nominal laser beam size at the film 66 is 60 micrometers FWHM (full width at half maximum) in the cross-scan direction and 40 micrometers (FWHM) in the in-scan direction.

## 2. Lenses L1 and L2

In Figure 9, the optical configuration of lens L1

are plano-convex cylinder lenses, and can be similar in size and shape, and in one embodiment generally rigid.

As shown in Figure 9, and described herein, the focusing direction of lens L1 and lens L2 are oriented  
5 generally perpendicular to each other. As such, lens L1 effects the shape of laser beam 88 in the cross-scan direction and lens L2 effects the shape of laser beam 88 in the in-scan direction.

Lens L1 and lens L2 are tilted or angled from a  
10 position which is perpendicular relative to the optical axis (or optical path) as defined by laser beam 88. By tilting lens L1 and lens L2, the reflected portion of laser beam 88, indicated as reflected beam 146 and reflected beam 147, can be controlled. In the  
15 exemplary embodiment shown, the reflected beam 146 is aimed and collected at absorbing surface 142 to avoid light scattering. The control of reflected beam 147 allows lens L1 to act as a beam splitter.  
Alternatively, reflected beam 147 could also be  
20 directed to a light absorbing surface. The reflected beam from both surfaces of L1 (the flat or planar surface and the convex surface), represented by reflected beam 147, is directed to the feedback sensor 140 which provides a feedback signal representative of  
25 the laser beam 88. The use of lens L1 as a beam splitter is described in detail later in the specification.

Referring to Fig. 9a, a perspective view illustrating an exemplary embodiment of lens L1 or lens  
30 L2 is shown for explanation of the orientation of lens L1 and L2, and the tilting of lens L1 or L2 relative to the optical path defined by laser beam 88. In particular, lens L1 includes a longitudinal axis 202a, a transverse axis 203a, and a normal axis 204a.  
35 Similarly, lens L2 includes a longitudinal axis 202b, a

203b are perpendicular to the optical path defined by laser beam 88. While transverse axis 203a and transverse axis 203b remain stationary, lens L1 and lens L2 are tilted or angled relative to the optical path 88 by rotating lens L1 about transverse axis 203a, and rotating lens L2 about transverse axis 203b. As such, longitudinal axis 203a is not perpendicular to the optical path 88, and longitudinal axis 203b is not perpendicular to the optical path 88.

The tilt of lens L2 serves a dual purpose. In addition to allowing reflected light to be dumped (or directed) onto the absorbing surface 142, it is possible to tune the focal length of the lens L2 by varying the angle of lens L2. L2 is rotatable about its transverse axis. A mechanism is provided for rotating lens L2 about its transverse axis. In particular, during the manufacturing and assembly of the optical scanner assembly 50, lens L2 can be rotated (or tilted); about an axis (its transverse axis) that is parallel to the in-scan direction of the laser beam 88, to change its focal length for tuning/calibrating the focal length of lens L2 to be positioned at film 66. In one exemplary embodiment, a rotation angle adjustment of lens L2 from 10° to 40° yields a focal length change of approximately 15%.

In Figure 10, a representative plot of one exemplary embodiment of the focal length of lens L2 relative to the tilt angle is shown. In this embodiment, lens L2 is a 150 mm lens. By adjusting the tilt angle of lens L2 (by rotating lens L2 about its transverse axis, wherein the tilt angle is defined as the angle between the longitudinal axis of lens L2 and a position wherein the longitudinal axis of lens L2 would be perpendicular to the optical path), the focal



conventional optical system, the method of compensating or adjusting for focal length variation of a lens similar to L2 would be to displace the lens along its optical axis. Such a method requires more physical  
5 space in the optical scanner assembly to allow for tuning adjustment and displacement of the lens. The novel technique in accordance with the present invention uses a simple plano-convex cylinder lens in which the focal point is adjusted or "tuned" through  
10 changing of the tilt angle of the lens. The transverse axis of lens L2 remains stationary. The present technique is useful for reducing the complexity of the optical scanner assembly design and maintains a compact size for the optical scanner assembly. Additional  
15 space within the optical scanner assembly for adjustment and displacement of the lens along the optical axis is no longer necessary.

Lens L1 and lens L2 have diffraction limited optical characteristics. As well known to those  
20 skilled in the art, since lens L1 and lens L2 have diffraction limited optical characteristics, they may be used to focus a laser beam on a scanned surface, wherein a predictable focus spot size (and position) is achieved across the scanned surface which can be  
25 calculated based on the physical characteristics of the lens. As used herein, the term "diffraction limited" can be defined as the property of an optical system, whereby only the effects of diffraction determine the quality of the image it produces. The term  
30 "diffraction limited lens" can be defined as a lens with aberrations corrected to the point that residual wave front errors are substantially less than 1/4 the wave length of the energy being acted upon. See, the Photonics Dictionary, 41st Edition, 1995 (Laurin

view of a cylinder lens is generally shown at 210. The cylinder lens 210 can be similar to cylinder lens L1 and/or cylinder lens L2. The cylinder lens 210 is a cylinder lens having a plano-convex optical shape.

5 Preferably, the cylinder lens is generally rigid. As such, the cylinder lens 210 includes a first, generally flat (or planar) surface 212 and a second, generally curved (or convex) surface 214. In one exemplary embodiment, the cylinder lens 210 includes a first  
10 substrate 216 and a second substrate 218, which are constructed of different materials. The first substrate 216 may be constructed/formed of glass and the second substrate 218 may be constructed/formed of a photopolymer. It is recognized that alternatively, the  
15 cylinder lens 210 can be formed of a unitary, solid molded material, such as glass. In one exemplary embodiment, the cylinder lens 210 (L2) first substrate 216 has a length of 25 mm and a width of 25 mm, and the second substrate 218 has a length of 15 mm and a width  
20 of 7.5 mm.

Cylinder lens 210 can be constructed/formed using a unique molding process. In one exemplary embodiment, cylinder lens 210 may be formed using the process steps shown in Figures 13, 14 and 15. In reference to Figure  
25 13, a mold 220 is provided having a top surface 222 which is curved corresponding to the desired curvature of the cylinder lens second curved surface 214 (for example, a concave surface will form a convex lens surface). In one exemplary embodiment, the mold 220  
30 may be formed of glass, wherein the curved top surface 272 is ground or diamond cut to the desired shape. The mold curved surface 222 is provided with a non-stick coating, indicated at 224. In one exemplary embodiment, a suitable non-stick coating is a Silane  
35 coating commercially available from PCB, Inc. in

photopolymer 228 which forms the cylinder lens second substrate 218. Dispenser 226 is operated to dispense UV curable photopolymer in discrete droplet form onto the mold 220 assembly including non-stick coating 224.

5 In one exemplary embodiment, the UV curable photopolymer is Summers Laboratory's J-91, located in Fort Washington, Pennsylvania. The dispenser 226 dispenses approximately 7 droplets per inch, having a droplet weight of approximately 1.5 mg.

10 In reference to Figure 14, the first substrate 216 is placed over the charged mold 220, sandwiching the UV curable photopolymer 228 between the first substrate 216 and the mold curved surface 222. In reference to Figure 15, a UV light source 230 is provided for curing  
15 the cylinder lens assembly 210. The UV light source 230 is positioned over the lens and mold assembly for an amount of time required for curing the photopolymer first substrate 216 onto the second substrate 218. After curing, the cylinder lens 210 may be removed from  
20 the mold 220. Due to the non-stick coating 224, the cylinder lens may be easily removed from the mold 220.

### 3. Laser Feedback Control System

The novel optical configuration of lens L1  
25 effectively allows lens L1 to be utilized as a "beam splitter" in a laser feedback control system. As previously stated herein, the tilting of lens L1 allows the reflected beam 147 of laser beam 88 to be directed to photosensor 140, such that it may be used in a  
30 feedback system for monitoring and stabilizing the laser assembly 76 (see, Figure 9 and Figure 9a). Although the lens L1 transverse axis remains perpendicular to the optical path defined by laser beam 88, the longitudinal axis is rotated about the

block diagram is generally shown at 240, showing lens L1 as a beam splitter in a laser feedback control system. As shown in Figure 16, and similar to operations previously described herein, laser assembly 5 76 emits (produces) laser beam 88 which is transmitted through lens L1. A portion of the laser beam 88 is reflected off the surface of lens L1, which has previously been described herein as reflected beam 147.

Due to the novel tilted configuration of lens L1, 10 reflected beam 147 is directed to the active region of photosensor 140. In one exemplary embodiment, 90% of the laser beam is transmitted through lens C1 and 10% of the laser beam is reflected to photosensor 140 as reflected beam 147.

15 Photosensor 140 is responsive to the reflected beam 147 for providing an output signal 242 to laser driver 74 which is representative of the power of the reflected beam 147. In response to feedback signal 242 and image signal 84, laser driver 74 provides modulated 20 output signal 86 to laser assembly 76.

In Figure 17, a top view of an exemplary embodiment of the use of the lens L1 in a laser feedback control system is shown at 244. As shown in Figure 17, cylinder lens L1 includes a top surface 246 25 and a bottom surface 248. The reflected beam 147 is comprised of reflections off of the cylinder lens top surface 246 (convex surface), indicated at 254, and bottom surface 248 (flat or planar surface), indicated at 252. Correspondingly, the photosensor 140 includes 30 an active region 250 which is large enough to receive the reflected beams 252, 254 from the top surface 246 and the bottom surface 248.

Laser assembly 76 emits a collimated light beam in the form of laser beam 88 which is transmitted through 35 lens L1. The reflected beam 147 represents the

particular, first reflected portion 252 is reflected from the cylinder lens bottom surface 248, and second reflected portion 254 is reflected from the cylinder lens top surface 246, onto the photosensor 140 active region 250.

In Figure 18, a side view of the lens feedback control system is shown at 256. In the cross-scan direction, reflected beam 252 from bottom surface 248 is reflected directly onto photosensor 140 (active region 250). The reflected beam is convergent from the top surface. In this configuration, the focal point is on reflected side. It is noted that since top surface 246 is convex shaped, the reflected beam 252 from top surface 246 reaches a focal point 255 approximately midway before it is incident onto the photosensor 140.

#### 4. Flexible Lens L3

In Figure 19, flexible lens L3 is generally shown in perspective view. In the exemplary embodiment shown, flexible lens L3 is a cylinder lens having a plano-convex optical shape. The flexible lens L3 is formed of a generally flexible material which allows flexible lens L3 to be easily shaped to a desired curvature, such as is required by the optical scanner assembly 60. The flexible lens L3 is flexible enough to be wrapped onto a guide. The flexible lens L3 is capable of being uniformly flexed beyond a 180° arc, while maintaining and exhibiting diffraction limited optical characteristics, and as such, allows the flexible lens L3 to be used in a laser imaging system suitable for medical applications.

In reference to Fig. 20, flexible lens L3 is a relatively thin, ribbon-like lens. Flexible lens L3 is a flexible, diffraction-limited lens which lends itself

arbitrary shapes, such as the 180° arc shown. In particular, flexible lens L3 can be utilized in one-dimensional laser scanning systems, in which a beam of light is scanned over a considerable distance (many  
5 inches), such as the laser imaging system shown in Figure 1. Referring to Fig. 21, flexible lens L3 can be flexed beyond a 180° arc, allowing the flexible lens L3 to be used in many applications which require the use of a flexible lens, either for obtaining desired  
10 optical characteristics or due to space constraints, without causing damage to the lens or damaging the optical characteristics of the lens. Flexible lens L3 is capable of being "flexed" or "bent" in over a 180° arc, while exhibiting and maintaining diffraction  
15 limited optical characteristics. As well known to those skilled in the art, by maintaining diffraction limited optical characteristics if a flexible lens in accordance with the present invention is used to focus a laser beam on a scanned surface, a predictable focus  
20 spot size (and position) is achieved across the scanned surface which can be calculated based on the physical characteristics of the lens. As used herein, the term "diffraction limited" can be defined as the property of an optical system, whereby only the effects of  
25 diffraction determine the quality of the image it produces. The term "diffraction limited lens" can be defined as a lens with aberrations corrected to the point that residual wavefront errors are substantially less than 1/4 the wavelength of the energy being acted  
30 upon. See, the Photonics Dictionary, 41st Edition, 1995 (Laurin Publishing, 1995).

Known conventional polygonal scanning systems often require the use of a rigid torodial or rigid cylinder shaped lens as part of field-flattening lenses

These lens have typically been ground out of glass, which do not lend themselves to being easily bent into arbitrary shapes. The novel flexible lens L3 in accordance with the present invention lends itself most readily to the production of long, positive cylinder lenses that can be easily bent into arbitrary shapes. Further, the method of construction described herein allows the construction of such lenses using a simple unique cast and cure system followed by using a simple guide for bending the flexible lens into the required shape for a desired application. It is recognized that an alternative method to construction of flexible lens L3 would be to injection-mold the lens out of plastic.

However, it is also recognized that creating long, diffraction-limited cylinder lenses of the type discussed herein would be quite difficult using injection molding processes.

In Figure 22, a cross-sectional view of a flexible cylinder lens is generally shown at 260. The flexible cylinder lens 260 can be similar to flexible lens L3 for use in an optical scanner assembly. In reference also to Figure 23, a longitudinal cross-sectional view of the flexible cylinder lens 260 is shown. In one exemplary embodiment, the flexible cylinder lens 260 is a multi-layered lens. The flexible cylinder lens 260 includes a first, optical substrate 262, a second, structural or support substrate 264, and a third, optical substrate 266. In the exemplary embodiment shown, first substrate 262 is formed of a photopolymer. Second substrate 264 is preferably a thin, flexible polymeric or plastic substrate. In one embodiment, it is recognized that the second substrate 264 may be formed of a polyester or polycarbonate. Additionally, the third substrate 266 may also be formed of a

length with a 3 mm high aperture. The photopolymer used for the first substrate 262 and the third substrate 266 is commercially available from Summers Laboratories under the tradename J-91. The second  
5 substrate 264 is formed of a .006 inch (.015 cm) thick layer of polycarbonate, having a 15mm by 251 mm substrate size.

In Figures 24-27, one preferred embodiment of forming flexible cylinder lens 260 is shown. In Figure  
10 24, a cylinder mold 270 is provided having a curved top surface 272 which corresponds to the desired shape of third substrate 266. In one preferred embodiment, the mold is made of glass, wherein the curved top surface 272 is ground to the desired shape. Alternatively, a  
15 non-glass mold can also be diamond turned to the desired shape. The cylinder mold 270 includes a non-stick coating 274 coated over the curved top surface 272. The non-stick coating 274 does not allow photopolymer to stick to the mold top surface 272. In  
20 one preferred embodiment, the non-stick coating 274 is a silane coating, commercially available from PCR, Inc.

A dispenser 276 is provided for dispensing photopolymer onto the mold top surface 272.  
25 Preferably, the dispenser 276 is a computer-controlled dispenser capable of dispensing a photopolymer material in the form of discrete droplets.

The cylinder mold 270 is charged operating the dispenser 276 to dispense discrete droplets of  
30 photopolymer, indicated at 278, onto the top surface 272. The discrete droplets 278 are sized and spaced to collect together into a layer, without voids or excess when the next substrate is positioned onto the mold 270. In one exemplary embodiment, the droplet are  
35 dispersed at a rate of 1 droplet per 2 mm, having a



Referring to Figure 25, the second substrate 264, formed of a flexible plastic, is positioned over the droplets 278 and laid onto the charged cylinder mold 270. In Figure 26, a UV light source 280 is provided.

5 Light source 280 is positioned over the resulting assembly 282 for a period of time required for curing the photopolymer 278 and mold assembly 282. At this stage, complete curing of the mold assembly is not necessary. It is recognized that the purpose of curing  
10 in this step is to avoid the lens being pulled away from the mold 270, which may occur if the entire flexible cylinder lens 260 were cast and cured at once.

Referring to Figure 27, the UV light source 280 is removed and the mold 270 is again charged. Dispenser  
15 276 is controlled for dispensing discrete photopolymer droplets onto the charged substrate 264 to form substrate 262.

Referring to Figure 28, a top mold substrate 284 is placed onto the molded construction over the  
20 dispensed droplets 282. In reference to Figure 29, the entire mold assembly is placed under UV light source 280 for a period of time required for complete curing of the mold assembly.

In reference to Figure 30, the top mold substrate  
25 284 is thin enough to allow it to flex, and has also been treated with a non-stick coating, such as a Silane coating. As such, the top mold substrate 284 may be easily "popped" off the cured molded construction for removal of finished flexible cylinder lens 260. In  
30 reference to Figure 29, it is recognized that external means 286 may be used for aiding in removal of the flexible cylinder lens 260 from the molded assembly, such as applying pressure to the molded assembly.

#### 5. Attenuator System

35 In Figure 32, an exemplary embodiment of the laser

include an attenuator 290. In one embodiment, the attenuator 290 is positioned between lens L1 and lens L2. Attenuator 290 is a variable density attenuator formed of a single unitary construction. The  
5 attenuator 290 may function to further shape laser beam 88, and in particular, for controlling and calibrating the power of laser beam 88 transmitted to the scanner mirror M2. Attenuator 290 is positioned between the laser mechanism and L2, and in the embodiment shown,  
10 adjacent L2. The unibody attenuation mechanism has a density gradient which is oriented perpendicular to the longitudinal axis of L2. The unique combination of the variable density attenuator 290 and L2 results in no change in the focusing of the laser beam at the focus  
15 spot on the photosensitive film.

Known attenuators used in conventional optical scanning systems utilize cross-polarizing attenuators.

Such attenuators include two polarized filters which  
are crossed for attenuating a laser beam passing  
20 through the crossed filter portion.

In Figure 33, a top view of one exemplary embodiment of the novel attenuator in accordance with the present invention is shown at 290. Attenuator 290 is a variable density attenuator, wherein the amount of  
25 laser beam attenuation varies (or increases) from first side 292 to second side 294, indicated by attenuation arrow 296. In Figure 34, a longitudinal cross section of attenuator 290 taken along line 34-34 of Figure 33 is shown. The attenuator 290 includes an attenuator  
30 substrate 298 having a varying reflective coating 300.

In one exemplary embodiment, the attenuator substrate 298 is formed of glass, and the attenuator coating 300 is a metallic coating, the thickness of which increases between first side 292 and second side 294.

therethrough. Further, the variable density unibody attenuator 290 is a linear density wedge. As such, the optical density of the attenuator mechanism 290 increases proportionally with the distance across the  
5 attenuator 290.

In operation, the attenuator top surface 302 is reflective (such as a mirror), not absorbing. As such, the farther one moves from first side 292 closer to second side 294, the more reflective (and less  
10 transmissive) attenuator 290 becomes. In Figure 35, a graph showing the plot of the optical density of one embodiment of attenuator 290 versus the distance or position longitudinally along attenuator 290 (indicated by density gradient directional arrow 296) is shown.  
15 As shown, the optical density representative of the amount of attenuation increases proportionally the farther one moves along the attenuator 290 in direction 296 (termed "density gradient").

In Figure 36, the effect of attenuator 290 on the  
20 position of laser beam 88 is shown (in the in-scan direction). The attenuator 290 density gradient is indicated by directional arrow 296. The attenuator density gradient is oriented perpendicular to the longitudinal axis of the second cylinder lens. As  
25 indicated at 310, the gaussian intensity profile of laser beam 88 is merely shifted by attenuator 290 as laser beam 88 passes through attenuator 290. It is recognized that since lens L2 is a plano-convex cylinder lens, the shifting of laser beam 88 by  
30 attenuator 290 does not effect the focusing of laser beam 88 onto the film 66. This unique optical configuration provides for the combination of a variable density attenuator 290 and L2 which results in no change in the focus spot at the photosensitive film  
35 positioned on the internal surface of the drum

passing through attenuator 290 is shown. As shown in Figure 37, the laser beam 88 is centered about axis 312. In Figure 38, laser beam 88 is shown at location 308 after passing through the attenuator 290. As such,  
5 it is noted that the shape of laser beam 88 has not changed, it has only shifted relative to central axis 312. In one exemplary embodiment of the optical scanner assembly in accordance with the present invention, the attenuator 290 shifts the laser beam 88  
10 100 microns.

In Figure 39, one exemplary embodiment for calibration of laser beam 88 using attenuator 290 is shown. As shown in Figure 39, the attenuator 290 is positioned for calibration of laser beam 88 during the  
15 manufacturing process of the optical scanner assembly 50. Calibration of the position of attenuator 290 is accomplished utilizing a motor 316 coupled to a controller 72. The motor 316 is electrically coupled  
20 coupled to attenuator 290, indicated by mechanical connection 320. Motor 316 is responsive to controller 72 for moving attenuator 290 a desired distance. In one exemplary embodiment, the motor 316 is a screw motor which is mechanically coupled to the optical  
25 scanner assembly 50.

In Fig. 40, a perspective view illustrating one exemplary embodiment of an optical scanner assembly in accordance with the present invention is generally shown. The optical scanner assembly 330 can be similar  
30 to the optical scanner assembly 50 described previously herein, and includes laser beam shaping and directing system 100. In particular, the optical scanner assembly 330 includes laser beam shaping and directing system 100 contained within an optical scanner housing

optics translation system 52.

The optical scanner housing 332 includes a flexible lens holder 334 having a guide 336, an optics module base 338 and a laser driver board enclosure 340.

5 The scanner motor 138 is positioned within the optical module base 338. Flexible lens L3 is located within flexible lens holder 334. In particular, flexible lens L3 is inserted within lens guide 336, which imparts a desired curvature (such as the 180° arc shown) to the  
10 flexible lens L3. The laser driver 74 is located within the laser driver board enclosure 340. Additionally, a scanner speed sensor 342 and start-of-scan detector 346 are coupled to the optical scanner housing 332.

15 In Fig. 41, another perspective view of the optical scanner 330 is shown. As shown in Fig. 41, the optical scanner housing 332 includes lens L2 holder 350, attenuator filter holder 352, and lens L1 holder 354. Accordingly, lens L2 is attached to optics module  
20 base 338 using lens L2 holder 350, attenuator 290 is attached to the optics module base 338 using attenuator filter holder 352, and lens L1 is attached to the optics module base 338 using lens L1 holder 354. Motor 316, as shown, is a linear actuator (e.g., screw motor)  
25 for adjusting the position of attenuator 352. The holders 350, 352 and 354 maintain lens L1, attenuator 290, and lens L2 in optical alignment along the optical path defined by laser beam 88 shown.

The optical scanner assembly in accordance with  
30 the present invention may be used in a laser imaging system which is suitable for use in medical imaging applications. Operation of such a system will be described in the following paragraphs. In reference to Fig. 1, the imaging system 30 can be a medical imaging

allows the photosensitive film to be moved between the film exposure assembly 34, the film processing station 36, and the film receiving area 38. The film supply mechanism 32 feeds a piece of film along the film transport path 44 into the film exposure assembly 34 for exposing a desired image on the photosensitive film using the optical scanner assembly in accordance with the present invention. After exposure of the desired image on the photosensitive film, the photosensitive film is moved along the film transport path 44 to the film processing station 36. The film processing station 36 develops the image (through the application of heat) on the photosensitive film. After film development, the photosensitive film is cooled and transported to the film receiving area 38, where it may be picked up by the laser imager operator.

Referring to Fig. 42, a block diagram illustrating one exemplary embodiment of operation of an optical scanner assembly in accordance with the present invention, located within a film exposure module, is shown. Referring also to Figs. 2 and 3, once a piece of photographic film 66 is positioned on the film platen 62, a desired image may be exposed on the film 66 using optical scanner assembly 50.

Digital image data 350 is input to controller 72, indicated at 352. The digital image data may be generated by magnetic resonance (MR), computed tomography (CT), or other types of scanners, as previously described herein. The digital image data is a sequence of digital image values representative of the image to be scanned. Upon receipt of the digital image data 350, controller 72 processes the digital image data to generate a sequence of digital laser drive values (i.e., exposure values), which are input to the laser driver 74 indicated as image signals 84.

photosensitive film 66, and as such, have been previously described herein as image signals 84.

Based on image signal 84 and a feedback signal 242 from photosensor 140, laser driver 74 provides a  
5 corresponding laser driver modulated output driver signal 86 to laser assembly 76 for producing laser beam 88 representative of the image to be exposed on the photographic film 66. Laser beam 88 passes through the optical scanner assembly laser beam shaping and  
10 directing system as previously described herein, which includes passing through first optical mechanism 78, attenuator 290, second optical mechanism 80, and scanning and directing system 82 for exposure of the desired image on the photosensitive film 66.

15 As previously described herein, first optical mechanism 78 (including lens L1 and flexible lens L3), and second optical mechanism 80 (including lens L2) function to shape the laser beam in two separate directions, which are perpendicular to each other. The  
20 first optical mechanism 78 functions to shape the laser beam 88 profile in a first direction (but not a second direction) for focusing the laser beam 88 in a first direction on the film 66, as previously described herein. Similarly, the second optical mechanism 80  
25 functions to shape the laser beam 88 in the second direction (but not the first direction) for focusing the laser beam 88 in the second direction on the photosensitive film 66. Further, first optical mechanism 78 provides a feedback signal 147 to photo  
30 sensor 140. Photo sensor 140 provides a feedback signal 242 to laser driver 74, representative of the laser beam 88. Based on feedback signal 242 and image signal 84, laser driver 74 provides modulated signal 86 to laser assembly 76. Attenuator 290 functions to  
35 further shape laser beam 88 as described herein for

Scanning and directing system 82 includes a scanner and mirror system for directing the laser beam 88 to the desired location on film 66 and scanning the laser beam 88 across the film 66 in a raster pattern  
5 for exposing the desired image on film 66. Controller 72 provides control signals 358 to scanning and directing system 82, and receives control signal 360, e.g., a start-of-scan signal, from detector 346 or speed signal from scanner speed sensor 342, from  
10 scanning and directing system 82. Similarly, optics translation system 52 receives control signals 362 from controller 72, and provides corresponding control signals 364 to controller 72. As previously described herein, within scanning and directing system 82, laser  
15 beam 88 is reflected by the folding mirror M1 such that it is incident on the scanner mirror M2. In one preferred embodiment, the scanner mirror M2 is a two-sided mirror which is mounted on the shaft through an adapter 137 of the scanner motor 138.

20 Upon operation of scanner motor 138, indicated by control signal 358, the scanner mirror M2 is rotated and the laser beam 88 is reflected outward radially, and transmitted through flexible lens L3 for exposing the film 66 in an image-wise raster pattern. Both  
25 sides of scanner mirror M2 are used for directing a laser beam 88 through flexible lens L3 to expose the film 66.

In one preferred embodiment, scanning and directing system 82 is a double scanning system. In  
30 particular, an image line is scanned twice with the same data on the photosensitive film 66. Double scanning has been found to improve image sharpness over single scanning, and makes scan line invisible under normal viewing conditions. The two scanned lines in an  
35 image line are scanned by the two sides of mirror M2



scanning and directing system 82 scans an image in a raster pattern on the photosensitive film 66, the optics translation system 52 moves the optical scanner assembly 50 along the longitudinal axis 56 of the drum 54, such that the entire image may be exposed on the film 66. In one preferred embodiment, the optics translation system cooperates with the optical scanner assembly 50 through controller 72 such that an image may be actively exposed on the film 66. As such, the optics translation system does not stop the optical scanner assembly 50 at the location of each scan line, and the optics translation system 52 is in a rest position during scanning of a scan line on the film 66 by the optical scanner assembly 50 (termed "continuous scanning operation" as known by those skilled in the art). The optics translation system 52 slowly moves the optical scanner assembly 50 in a uniform manner during scanning of the image scanned lines on the photosensitive film 66. In this embodiment, the image scan lines do not run perpendicular to the longitudinal axis of the drum 56, but rather results in an image formed by scan lines which are approximately perpendicular to the longitudinal axis 56 of the drum 54.

Upon completion of exposure of the desire image or images on film 66 by the optical scanner assembly 50, optical scanner assembly 50 is moved to a start position by optics translation system 52, ready for exposure of another image on another piece of film. The exposed photosensitive film 66 is transported from the exposure module 34 using film transport system 40 to the film processing station 36 for thermal processing of the photosensitive film as previously described herein.

Having described the exemplary embodiments of the

consideration of the specification and practice of the invention disclosed herein. For example, the scanning assembly in accordance with the present invention may be used in other laser scanning application, such as  
5 film digitization. Therefore, the specification and examples should be considered exemplary only.

**What is claimed is:**

1. A feedback system (244) for providing a feedback signal representative of a laser beam (88) focused along an optical path onto a scanning surface (66), the feedback system (244) comprising:
  - a cylinder lens (L1) having a longitudinal axis (202a) and a transverse axis (203a), located along the optical path having an optical surface for shaping and focusing the laser beam (88) in a first direction; and
  - a photodetector (140) having an active region (250) sensitive to light;wherein the laser beam (88) includes a scanning portion which passes through the cylinder lens (L1) and a reflected portion (247) which reflects off the cylinder lens (L1), wherein the reflected portion (247) is reflected such that it is incident on the photodetector active region (250).
2. The system (244) of claim 1, further wherein the photodetector active region (250) is responsive to the reflected portion (247) for providing an output signal representative of the laser beam (88).
3. The system (244) of claim 1 or 2, wherein the lens (L1) is angled such that the reflected portion (247) is incident on the active region (250).
4. The system (244) of any of claims 1-3, wherein the cylinder lens (L1) transverse axis (203a) is perpendicular to the optical path, and wherein the cylinder lens (L1) longitudinal axis (202a) is not perpendicular to the optical path.
5. The system (244) of any of claims 1-4

6. The system (244) of any of claims 1-5, wherein the lens (L1) includes a flat partially reflective surface (248) and a curved partially reflective surface (246), and the curved surface is  
5 between the flat surface (248) and the scanning surface (66), and wherein the reflected portion (247) includes a first reflected beam (252) reflecting from the flat partially reflective surface (248) and a second  
10 reflected beam (254) reflecting from the curved, partially reflective surface (246).

7. The system (244) of any of claims 1-6, further comprising a second cylinder lens (L2) located  
15 along the optical path oriented generally perpendicular to the cylinder lens (L1) for shaping and focusing the laser beam (88) in a second direction.

8. A laser feedback control system for use in a  
20 laser imaging system (30), the laser feedback control system including a feedback system (244) according to any of claims 1-7, and further comprising:

a laser assembly (76) for producing the laser beam (88) representative of an image to be exposed  
25 on film (66).

9. The system of claim 8, further comprising a laser driver (74), wherein the laser driver (74) is responsive to the output signal for providing a  
30 modulated laser beam output signal (86).

10. The system of claim 9, further comprising a controller (72), wherein the controller (72) provides an image signal (84) to the laser driver (74), wherein  
35 the laser driver (74) is responsive to the output

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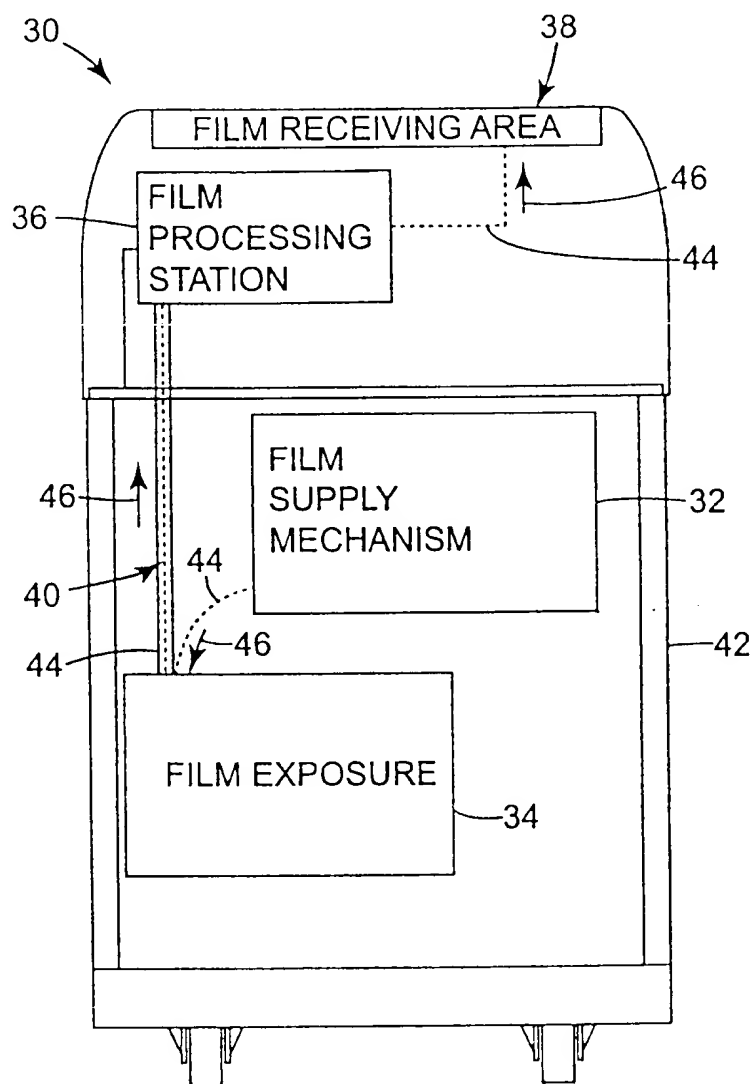


Fig. 1

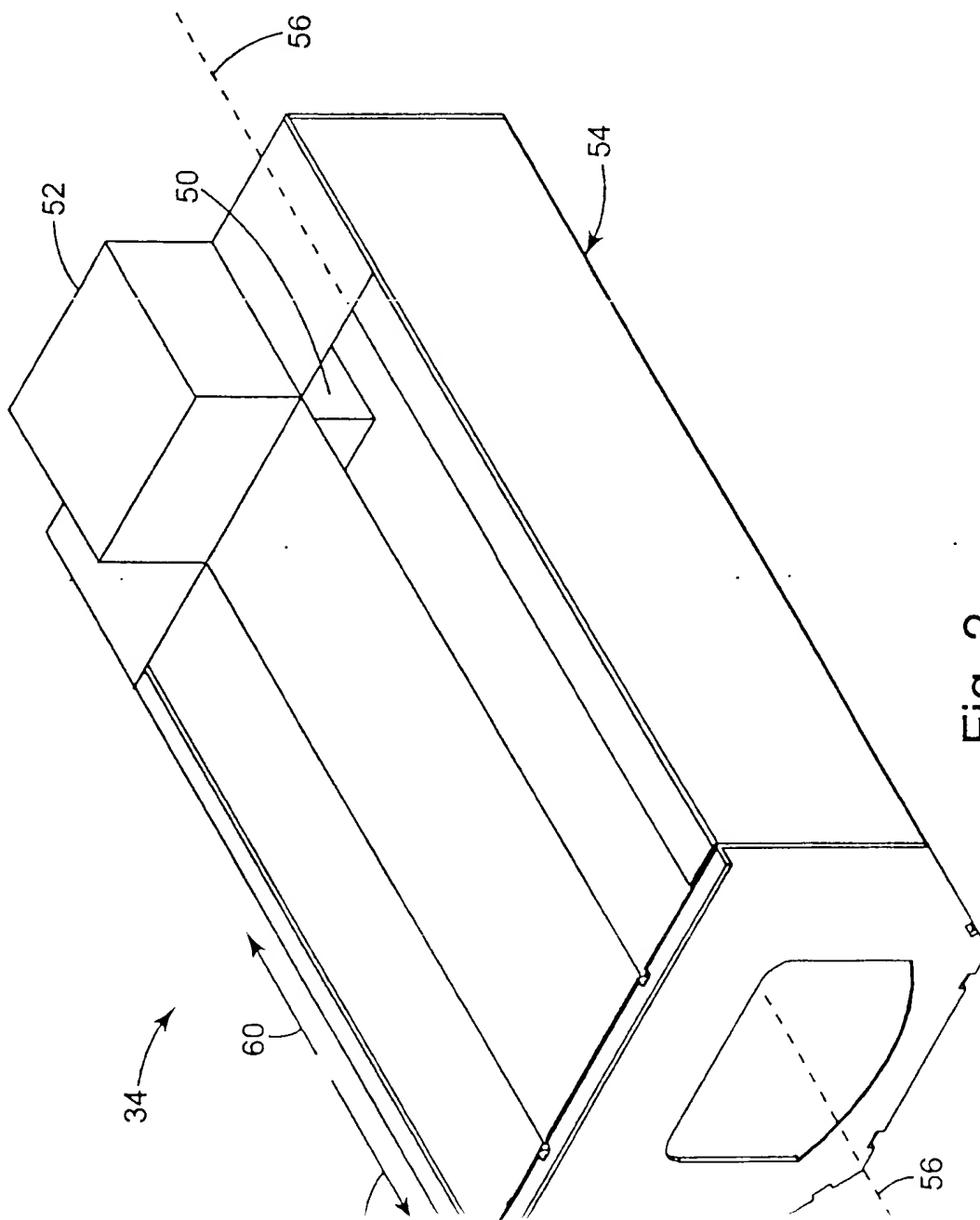


Fig. 2

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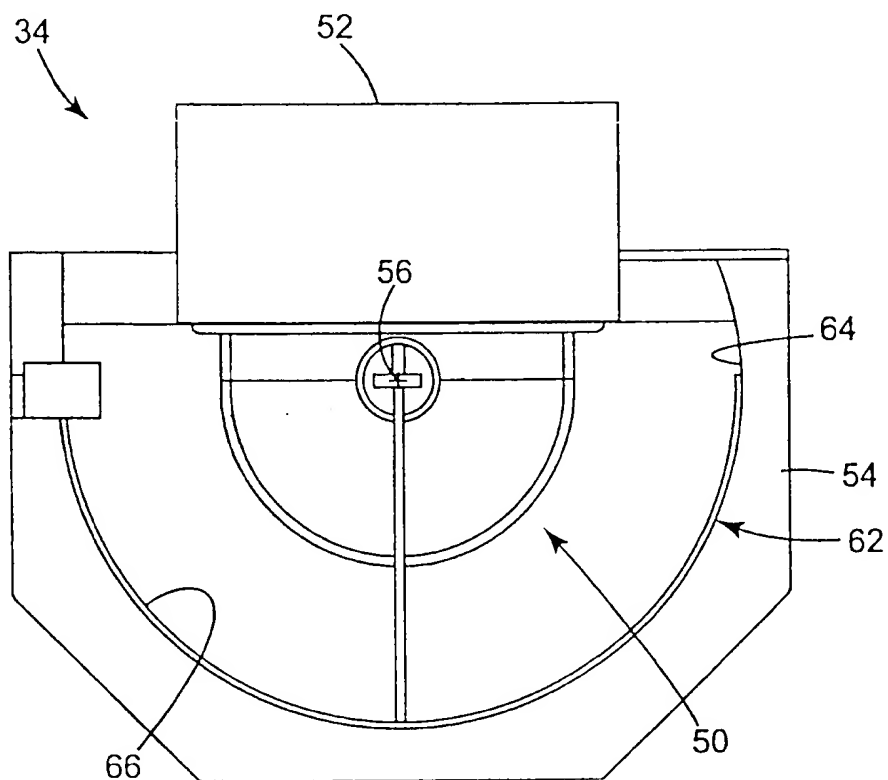


Fig. 3

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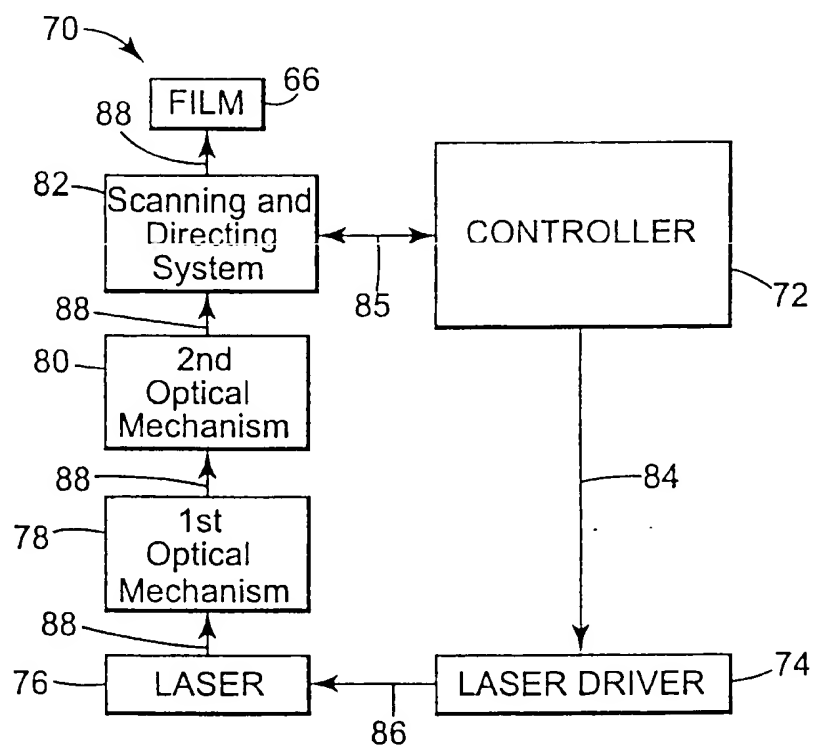
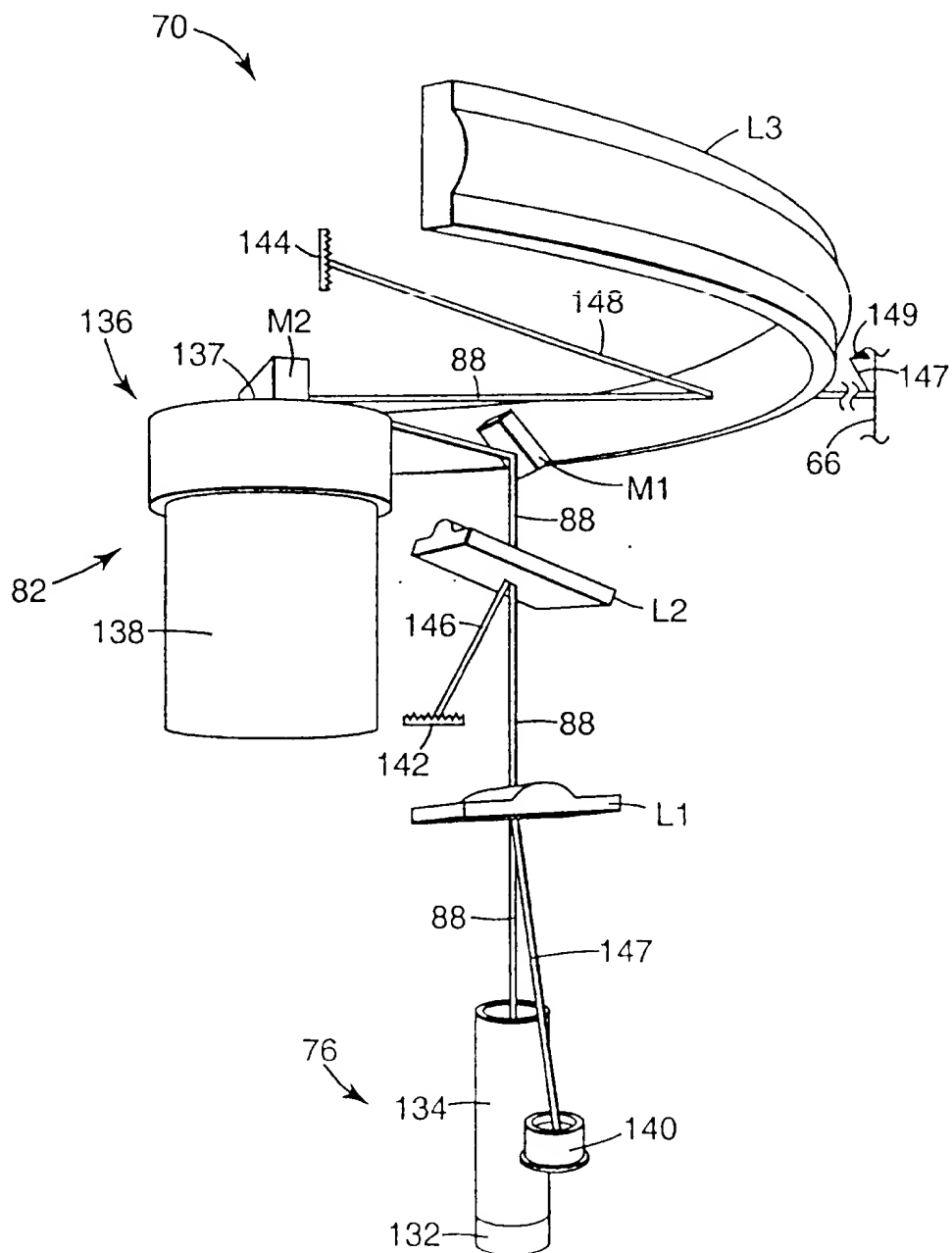


Fig. 4



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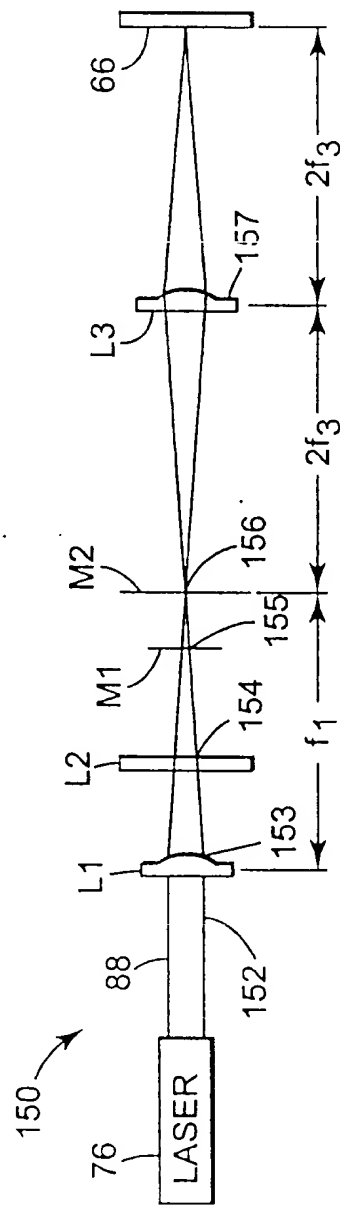


Fig. 6

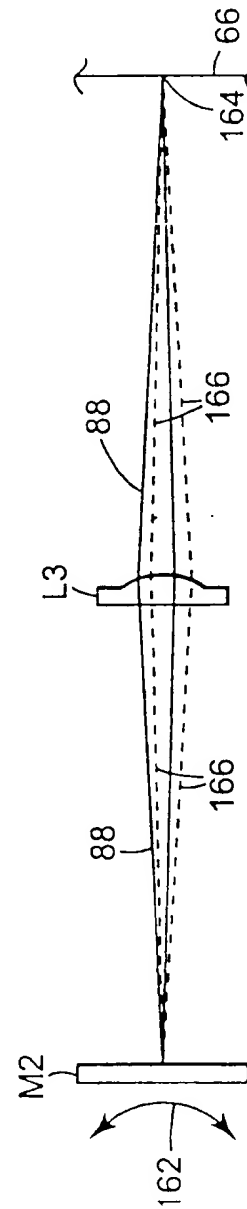


Fig. 7

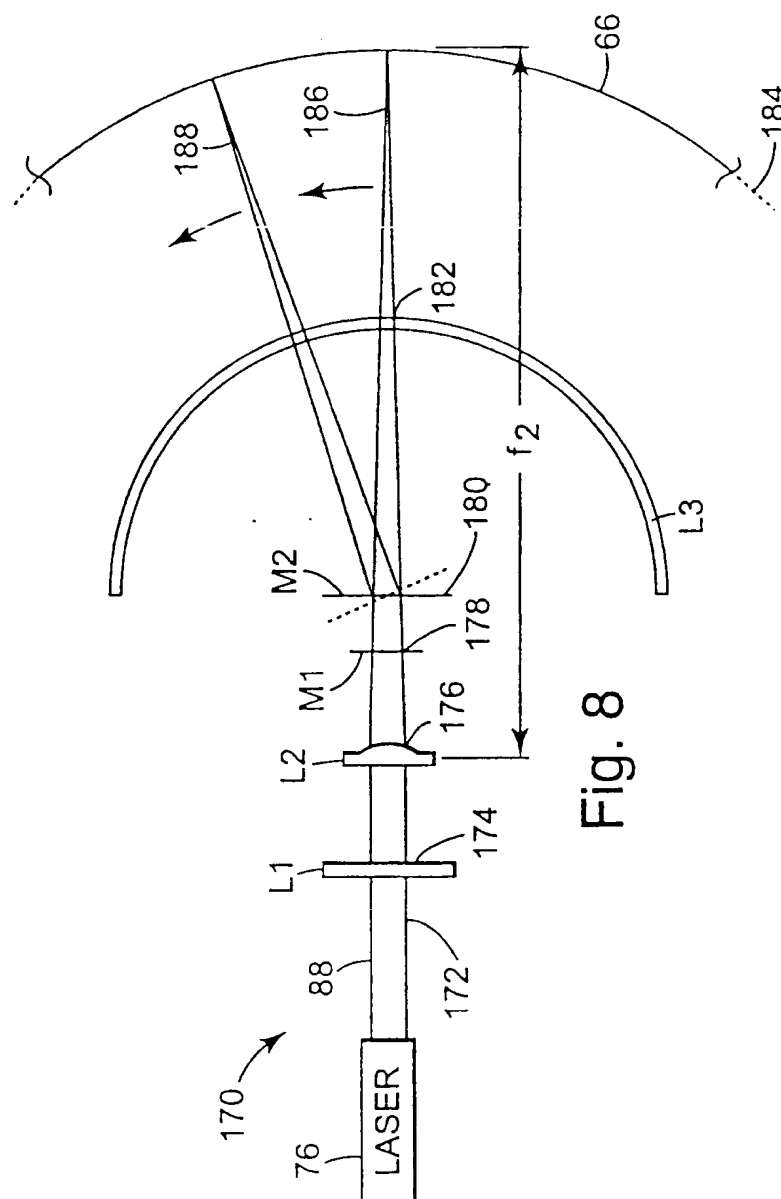


Fig. 8

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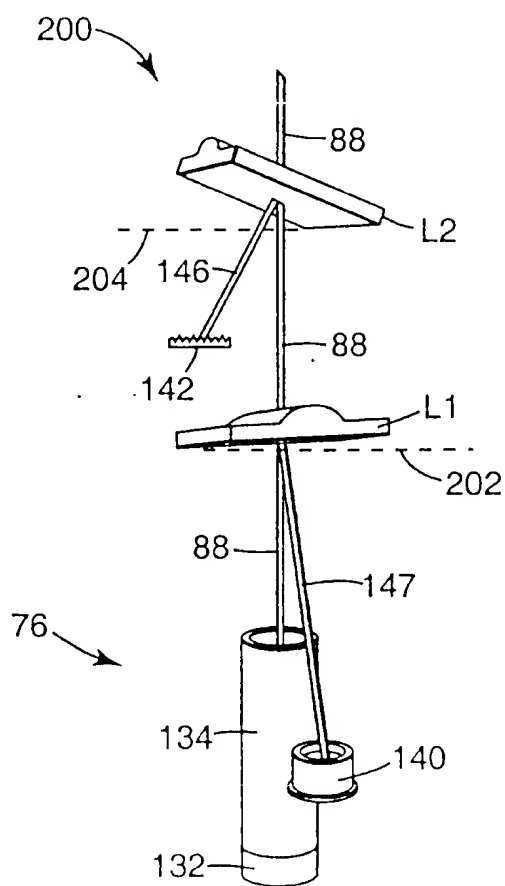
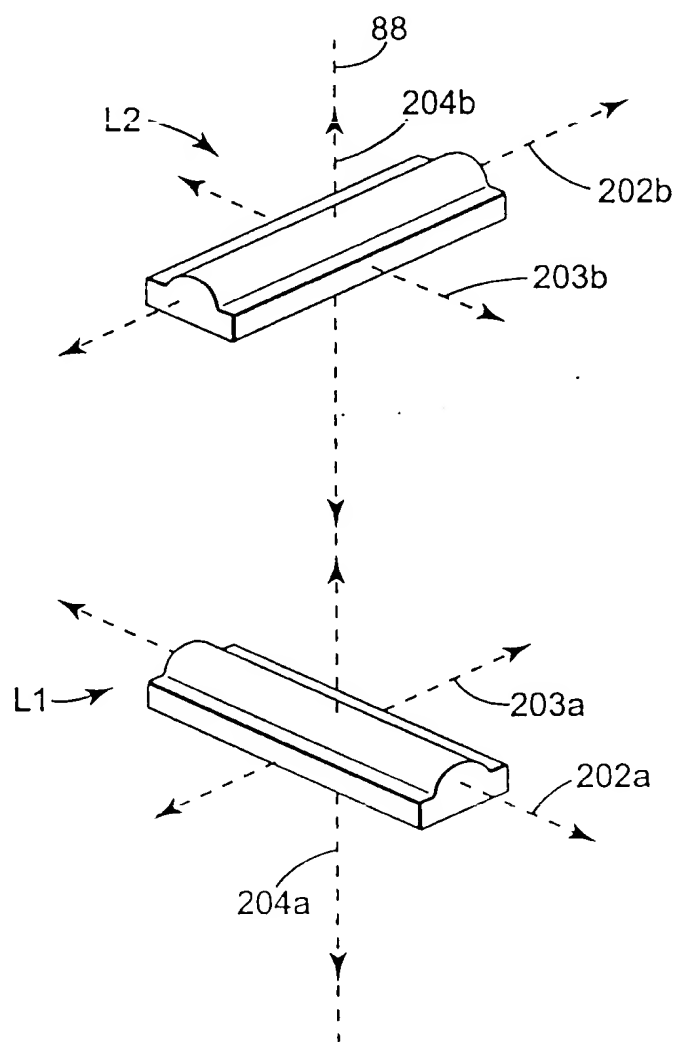


Fig. 9

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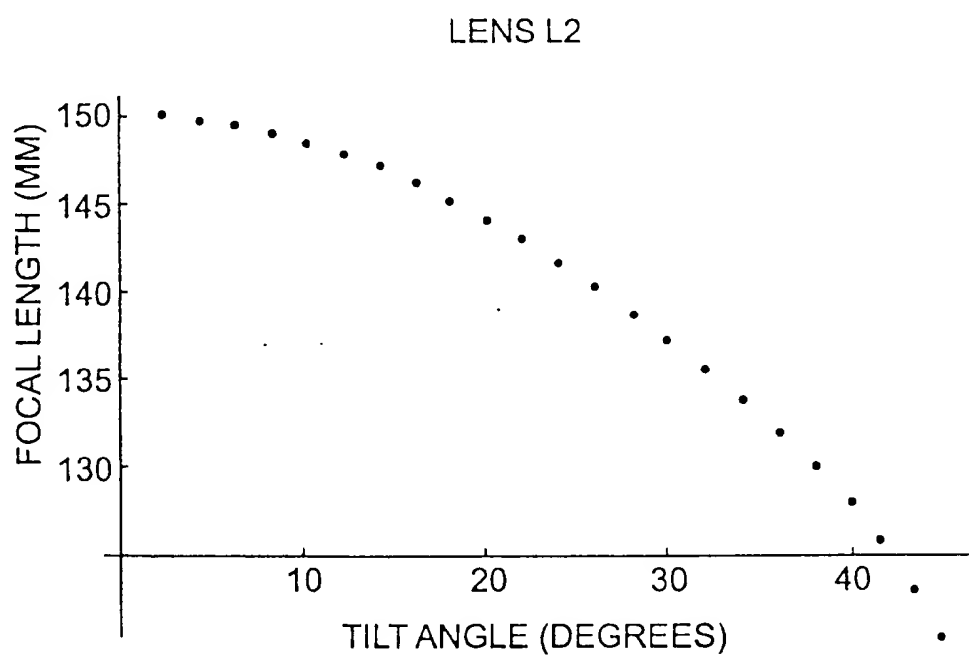


Fig. 10

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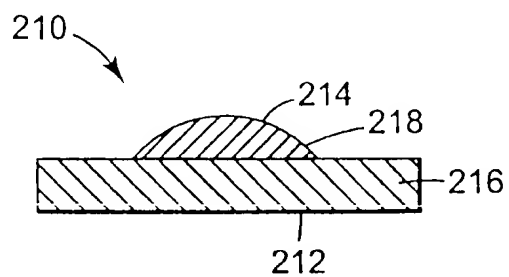


Fig. 11

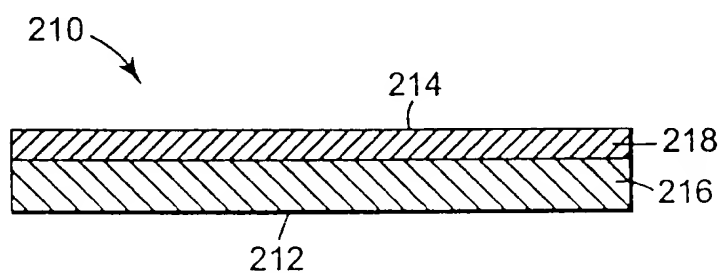


Fig. 12

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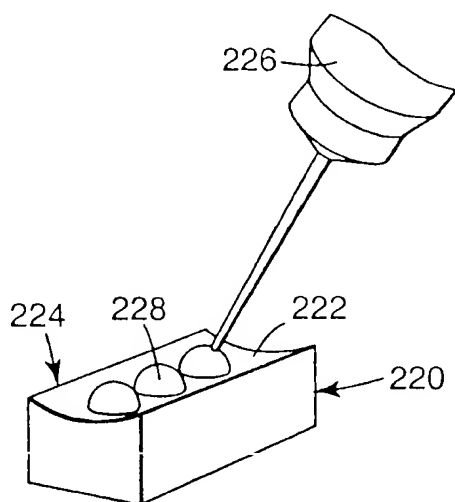


Fig. 13

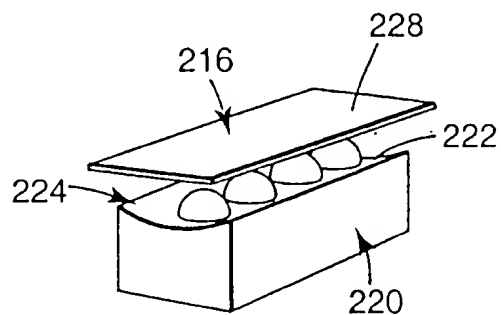
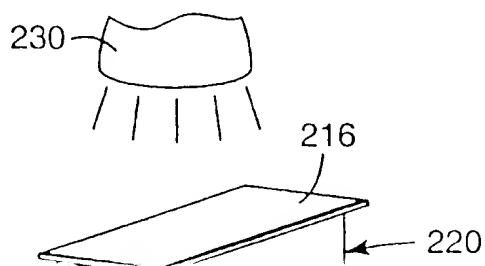


Fig. 14



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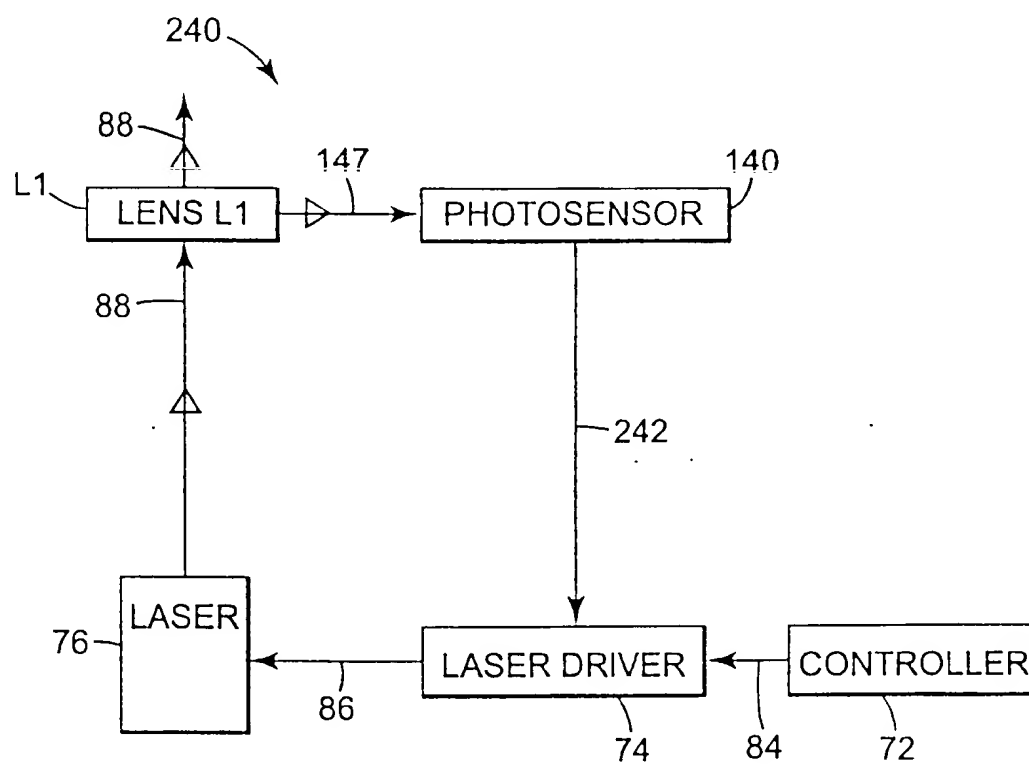


Fig. 16

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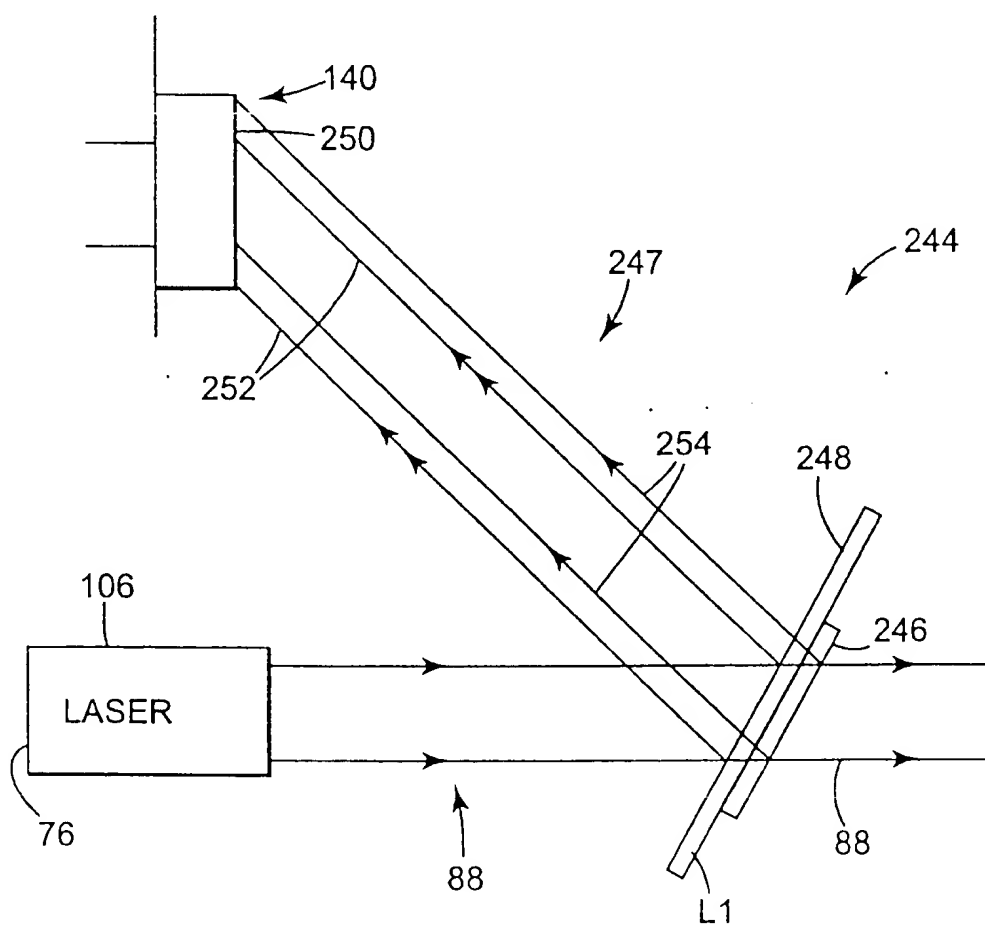


Fig. 17

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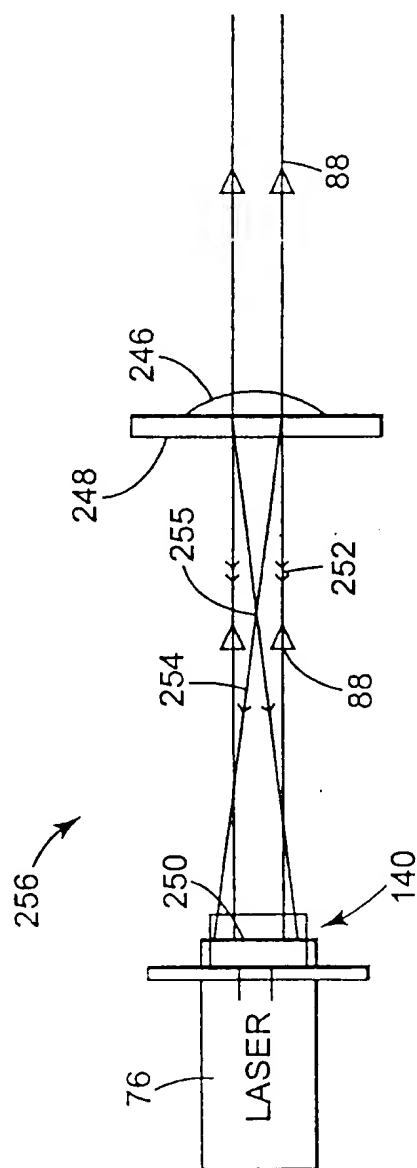


Fig. 18

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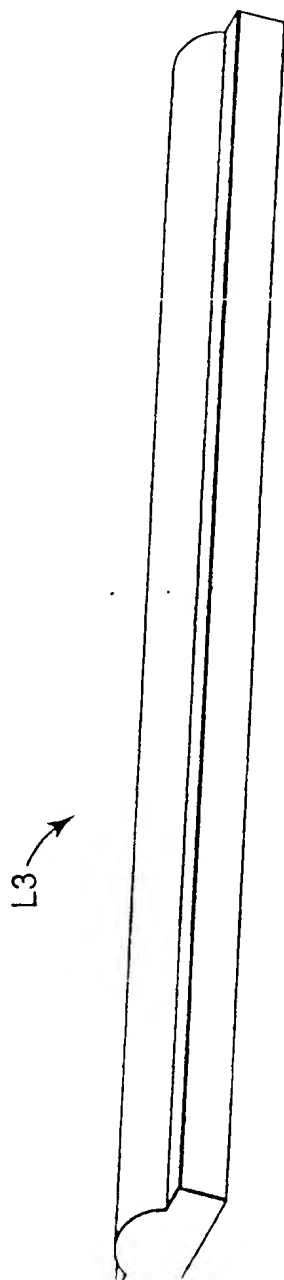


Fig. 19

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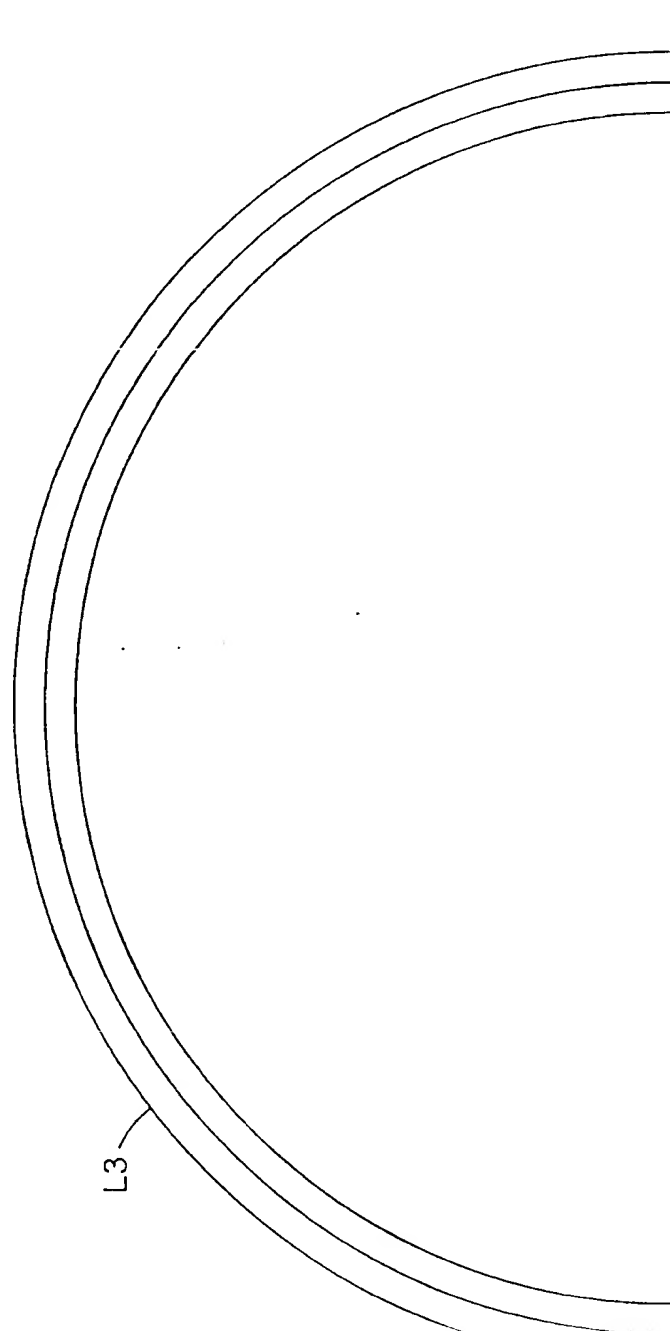


Fig. 20

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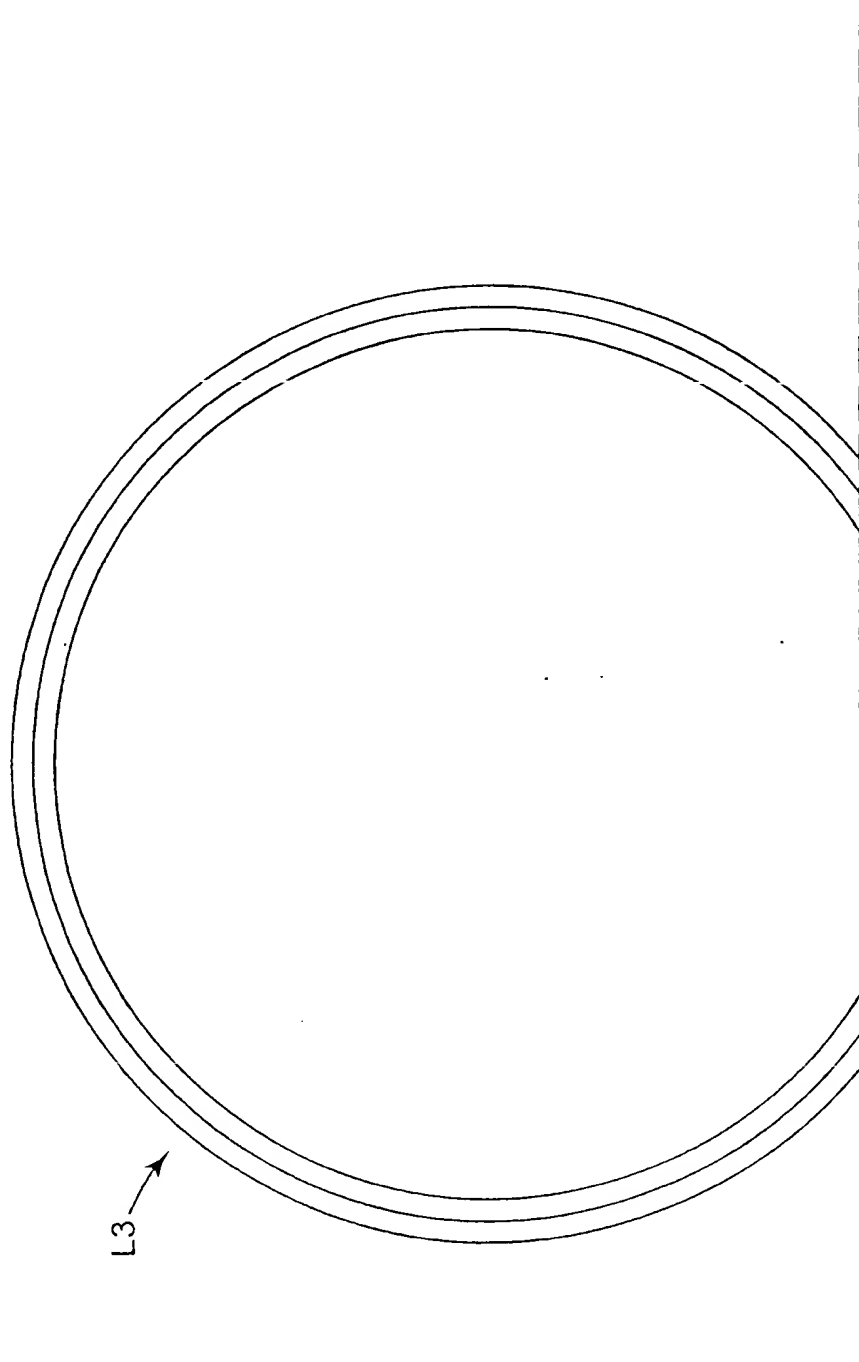


Fig. 21

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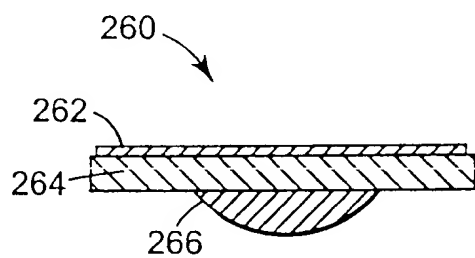


Fig. 22

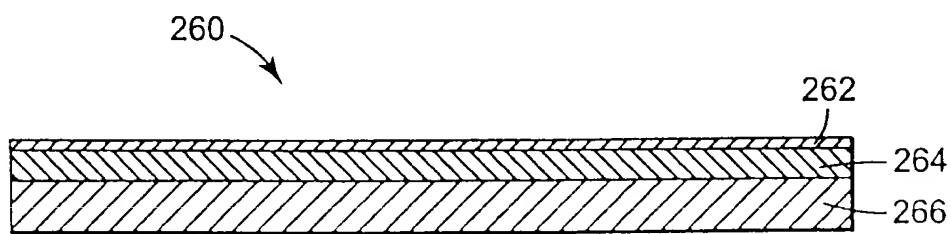


Fig. 23

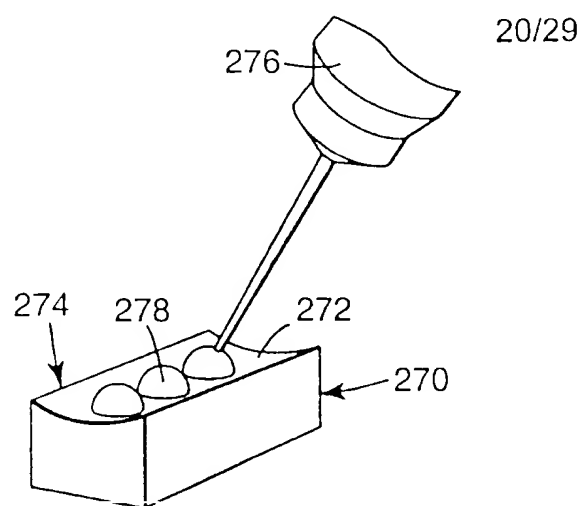


Fig. 24

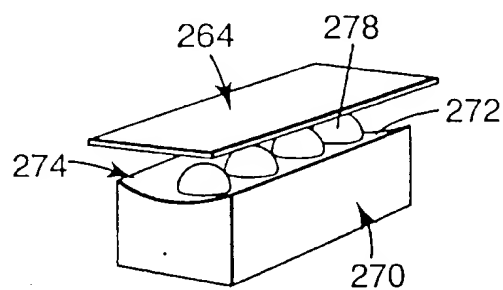


Fig. 25

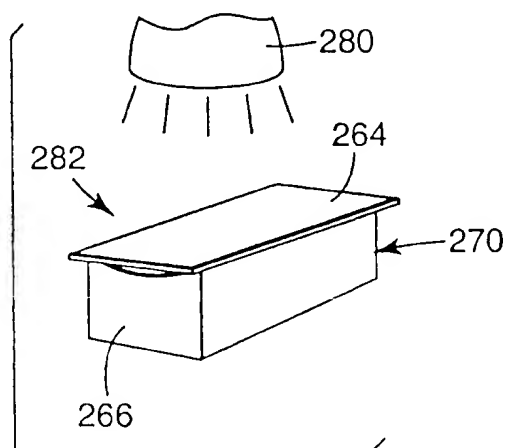


Fig. 26

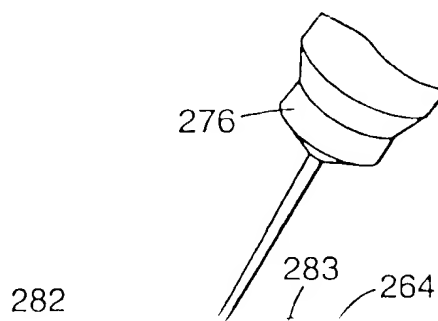


Fig. 27



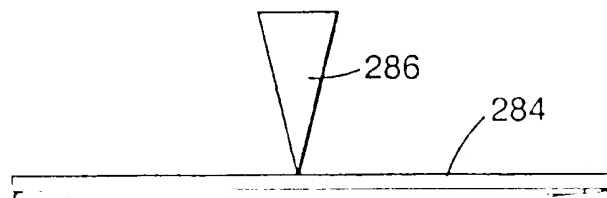
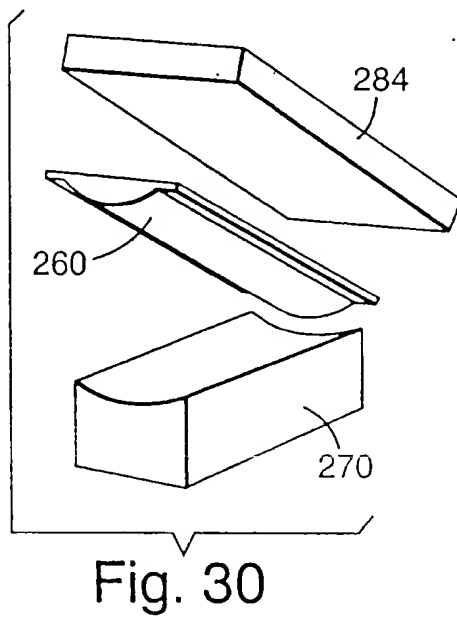
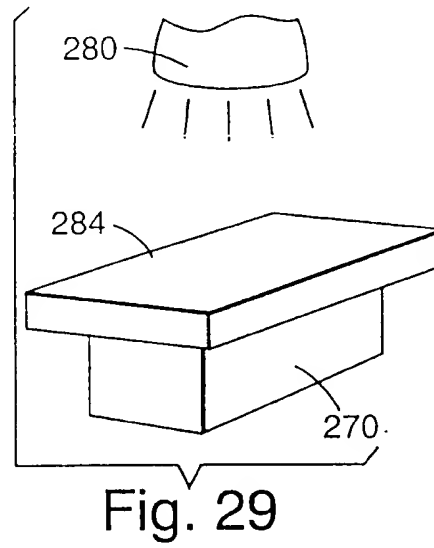
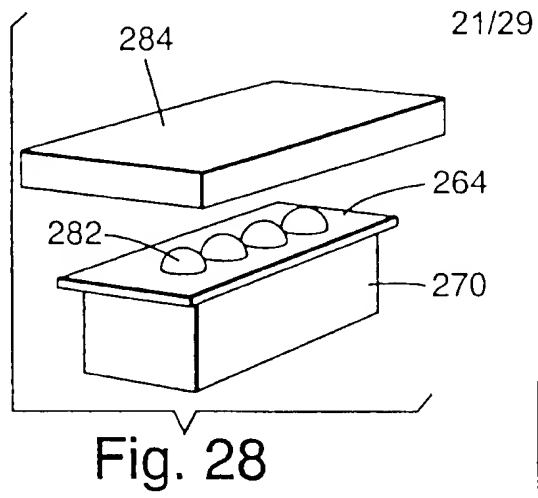
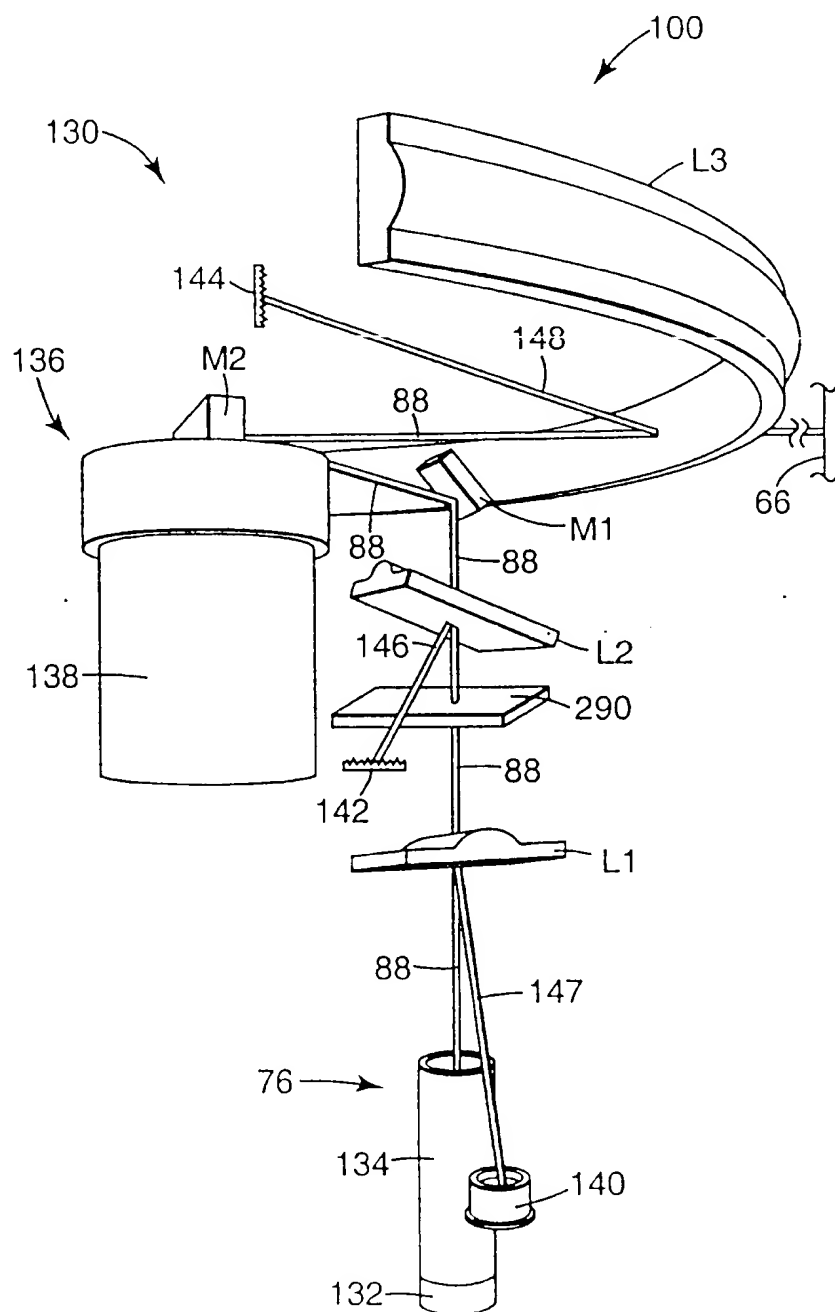
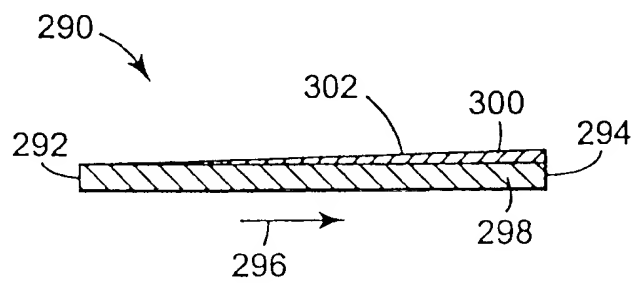
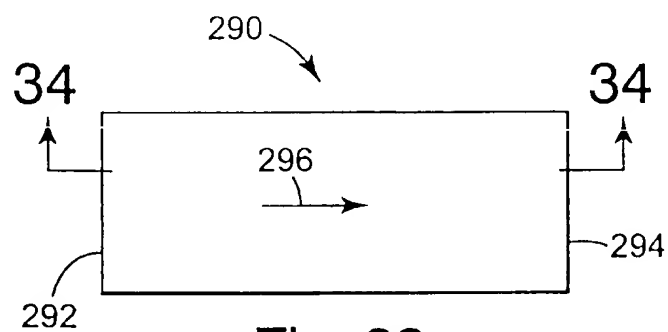


Fig. 31

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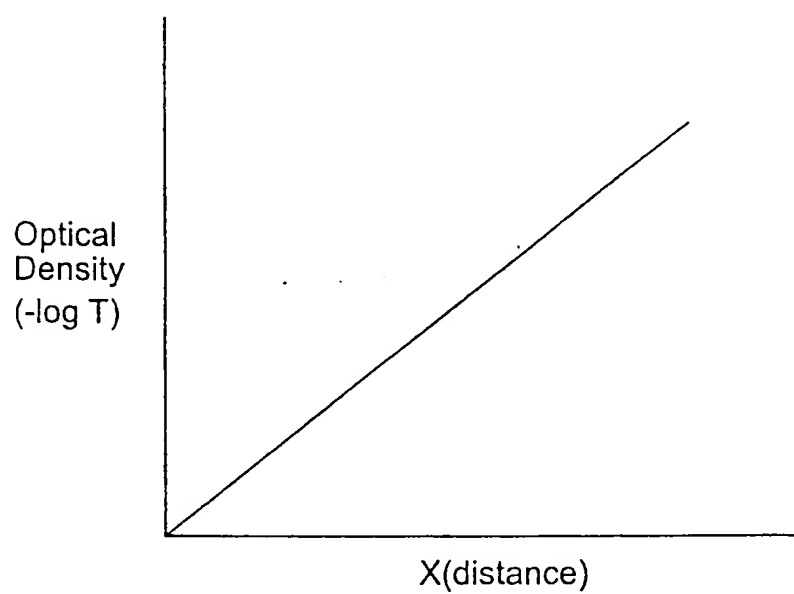


Fig. 35

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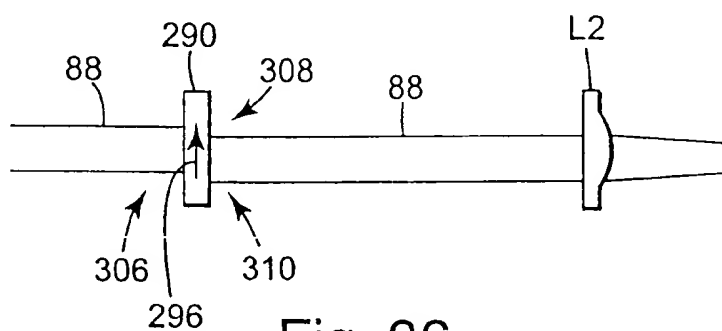


Fig. 36

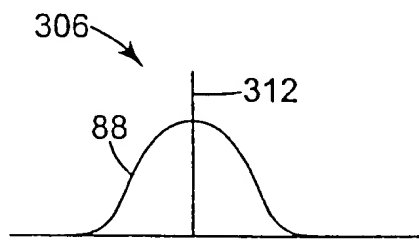


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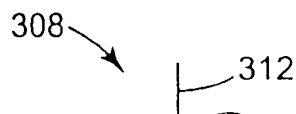


Fig. 38

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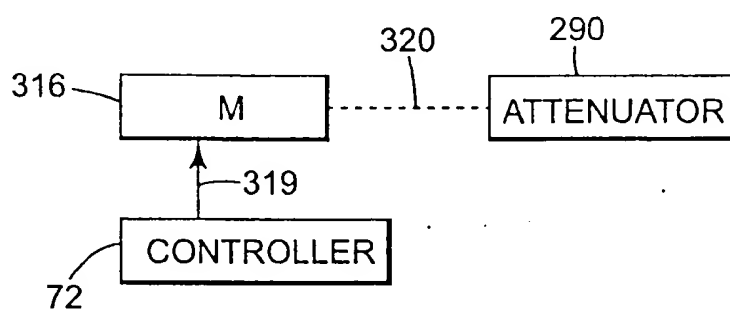


Fig. 39

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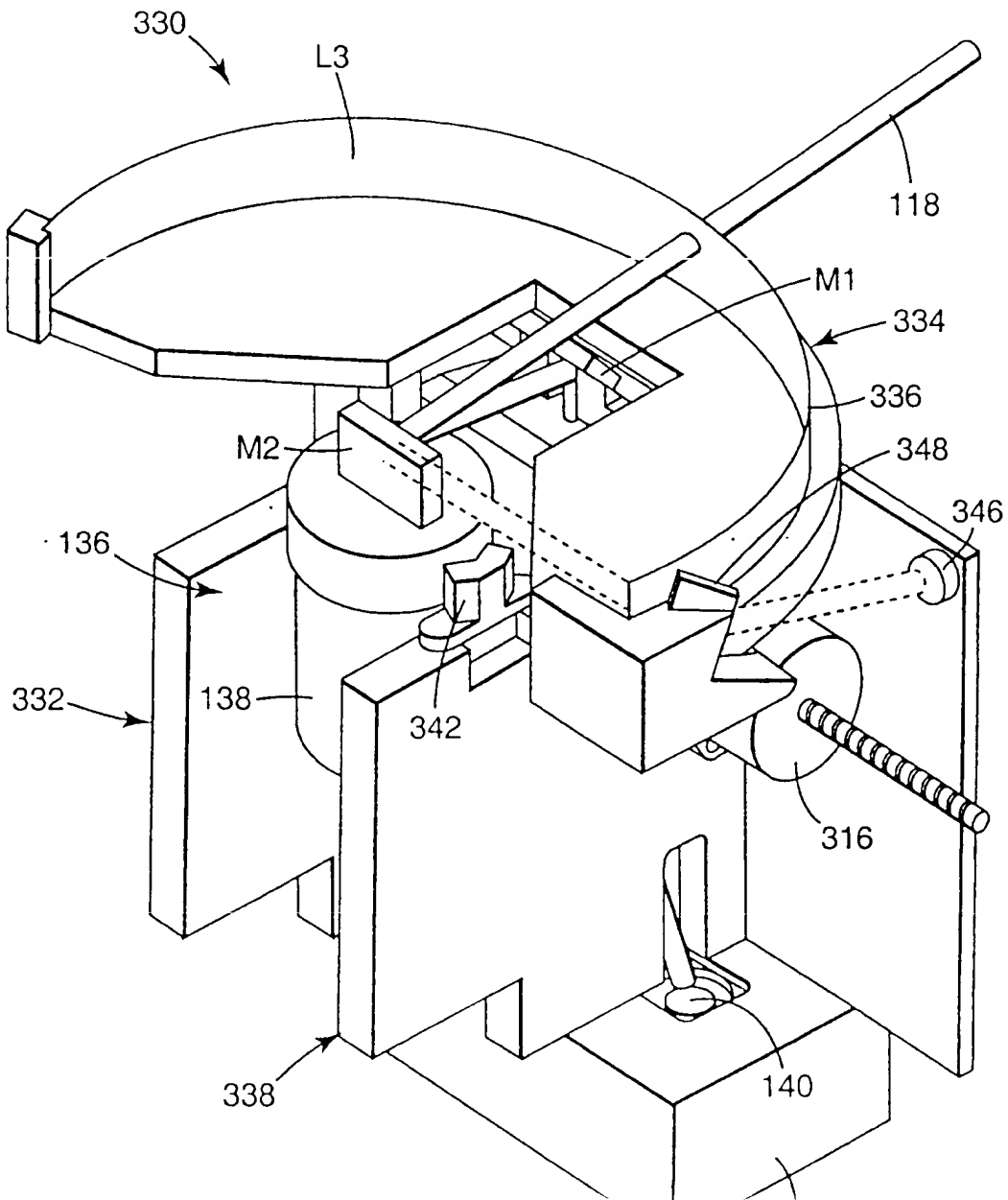


Fig. 40

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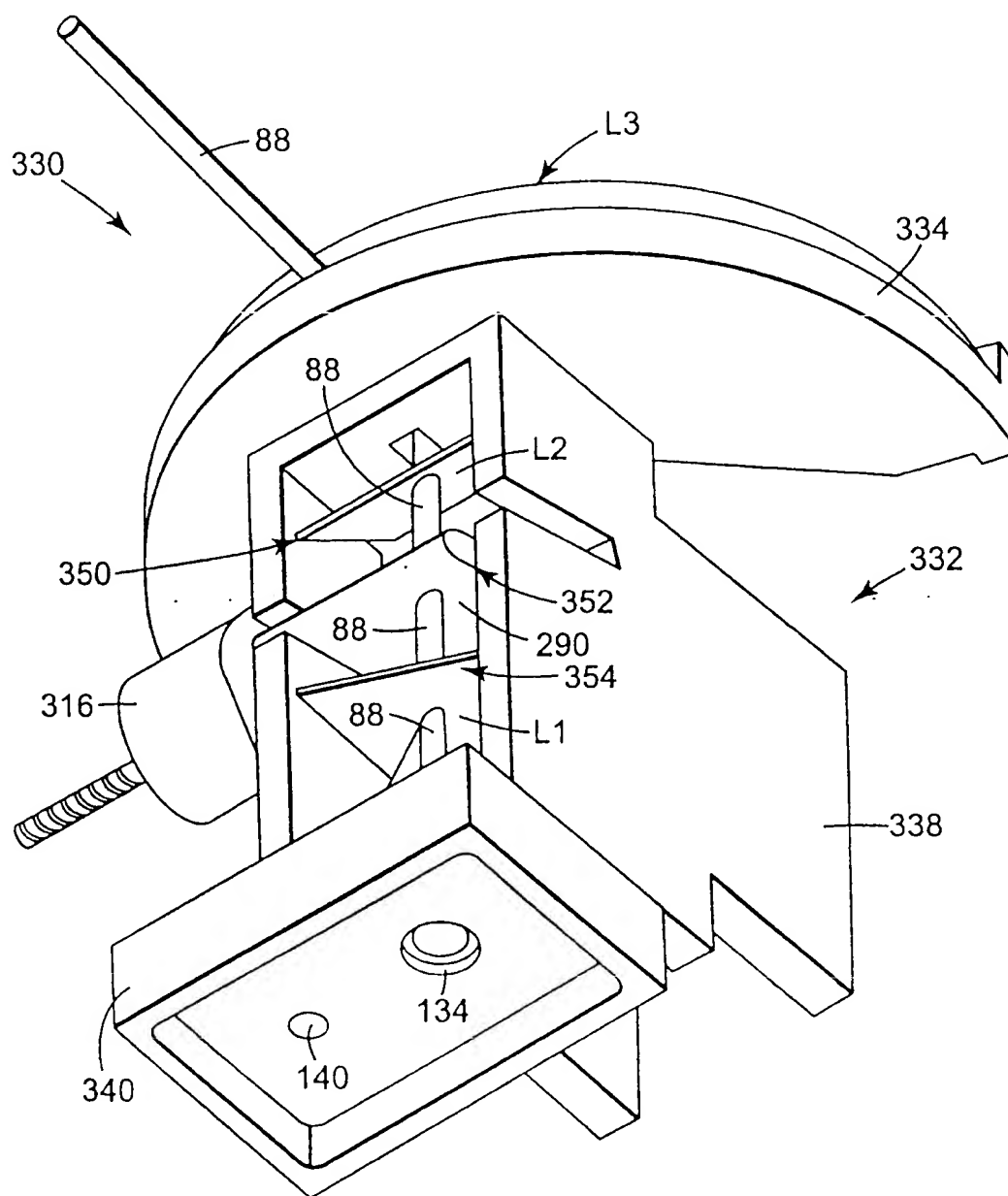
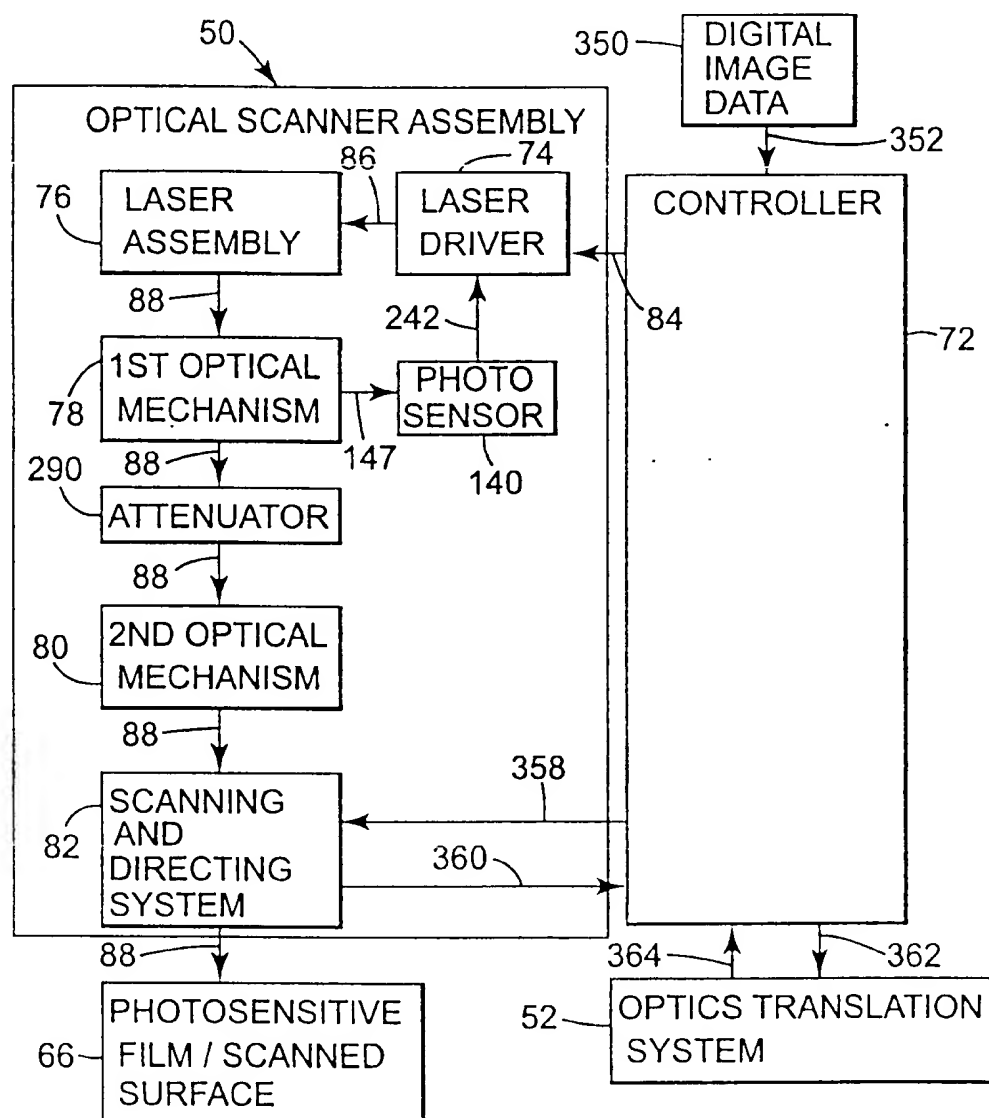


Fig. 11



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## INTERNATIONAL SEARCH REPORT

International application No.

PCT/US 98/18890

## A. CLASSIFICATION OF SUBJECT MATTER

IPC6: G02B 26/10, G02B 26/12, G02B 27/10

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC6: G02B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPODOC

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP 0550237 A1 (XEROX CORPORATION), 7 July 1993 (07.07.93), figures 1,5,6, claims 1-3 --	1,3,4-7
A	Derwent's abstract, No 91-191426/26, week 9126, ABSTRACT OF SU, 1583912 (AS BELO TECH CYBERNETICS), 5 April 1988 (05.04.88) --	8-10
A	Derwent's abstract, No 92- 78395/10, week 9210, ABSTRACT OF SU, 1654768 (AS USSR SPACE RES), 16 May 1989 (16.05.89) --	1,6
A	US 5237444 A (SCHERMER), 17 August 1993 (17.08.93), claims 1,4 --	1,3,6



Further documents are listed in the continuation of Box C.



See patent family annex.

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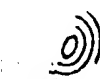
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Igor Gazdik

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## C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Form PC-15A 210 (continuation of second sheet) (July 1992)

# INTERNATIONAL SEARCH REPORT

Information on patent family members

03/11/98

International application No.

PCT/US 98/18890

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP 0550237 A1	07/07/93	DE 69213198 D,T JP 5249401 A US 5208701 A	06/02/97 28/09/93 04/05/93
US 5237444 A	17/08/93	NONE	
US 5475522 A	12/12/95	JP 6043370 A	18/02/94